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Phase Equilibria and Crystal Chemistry in Portions of the System SrO-CaO-Bi₂O₃-CuO, Part II—The System SrO-Bi₂O₃-CuO

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National Institute of Standards and Technology, Gaithersburg, MD 20899 New data are presented on the phase equilibria and crystal chemistry of the binary systems SrO-Bi₂O₃ and SrO-CuO and the ternary system SrO-Bi₂O₃-CuO. Symmetry data and unit cell dimensions based on single crystal and powder xray diffraction measurements are reported for all the binary SrO-Bi₂O₃ phases, including a new phase identified as Sr₆Bi₂O₉. The ternary system contains at least four ternary phases which can be formed in air at ~900 °C. These are identified as Sr₂Bi₂CuO₆, Sr₈Bi₄Cu₅O_{19+x}, Sr₃Bi₂Cu₂O₈ and a solid solution (the Raveau phase) which, for equilibrium conditions at ~900 °C, corresponds approximately to the formula

 $Sr_{1.8-x}Bi_{2.2+x}Cu_{1\pm x/2}O_x$ (0.0 $\leq x \leq \sim$ 0.15). Superconductivity in this phase apparently occurs only in compositions that correspond to negative values of x. Compositions that lie outside the equilibrium Raveau-phase field often form nearly homogeneous Raveau-phase products. Typically this occurs after relatively brief heat treatments, or in crystallization of a quenched melt.

Key words: crystal chemistry; phase equilibria; single crystal diffraction; SrO-CaO-Bi₂O₃-CuO; superconductivity; x-ray powder diffraction.

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1. Introduction

The discovery of high transition temperature (T_c) superconductivity in cuprates by Bednorz and Müller [1] and its confirmation by Takagi et al. [2] as being due to the phase La_{2-x}Ba_xCuO₄ led to a world-wide search for other compounds with higher T_c . These researches first produced La_{2-x} Sr_x CuO₄ [3] and quickly led to the discovery of a mixed phase composition in the system BaO- Y_2O_3 -CuO with a $T_c \sim 90$ K [4], well above liquid nitrogen temperature (73 K). Identification of the superconducting phase as Ba₂YCu₃O_{6+x} [5] has resulted in hundreds of published reports on the properties of this phase. Our own phase equilibria studies of the system BaO-Y₂O₃-CuO [6,7] have shown that CO2 is an important constituent of bulk ceramics that are prepared in air.

Phases with still higher T_c were found in the systems SrO-CaO-Bi₂O₃-CuO and BaO-CaO-Tl₂O₃-CuO [8,9]. These phases belong mostly to a homologous series $A_2Ca_{n-1}B_2Cu_nO_{2n+4}$ (A = Sr, Ba; B= Bi, Tl) although another series $A_2Ca_{n-1}BCu_nO_{2n+3}$ (A=Ba, B=Tl) can also lead to superconducting phases [10]. Still other compounds have been discovered with high T_c , i.e., $Pb_2Sr_2YCu_3O_{8+\delta}$ [11], $Ba_{1-x}K_xBiO_3$ [12] (with no Cu ions!) and Nd_{2-x}Ce_xCuO₄ [13]. The Tl⁺³ containing phases with the largest values of n, so far have the highest confirmed T_c , up to ~ 125 K [9]. However, the phases in the Tl+3 system are difficult to prepare as bulk single phase samples, and the relevant phase equilibria have not been determined, owing to the extreme volatility of Tl and

the poisonous nature of Tl vapors. In the Bi+3 containing systems the phase with n=2 and $T_c \sim 80$ K is easily prepared. However, its exact single-phase region is not well known and a structure determination has not been completed because of very strong incommensurate diffraction that is apparently due to a modulation of the Bi positions. Higher n (and higher T_c) phases have not been prepared as single phase bulk specimens (without PbO). Thus, we undertook a comprehensive study of the phase equilibria and crystal chemistry of the entire four component system SrO-CaO-Bi₂O₃-CuO. It is hoped that a complete understanding of the crystal chemistry and thermodynamics of the many phases formed will lead to a better understanding of the processing parameters for the preparation of bulk ceramics with reproducible and useful properties.

A prerequisite to understanding the phase equilibria of the four-component system is adequate definition of the phase relations in the bounding binary and ternary systems. The ternary system SrO-CaO-CuO was the first to be investigated and the results were published separately [14]. The solubilities of CaO in the solid solutions that are based on SrO:CuO phases were determined, and a ternary phase Ca_{1-x} Sr_xCuO_2 (x=0.14-0.16) was discovered. The structure of this ternary phase was refined by Siegrist et al. [15]. The present paper discusses the experimental determination of the phase relations and crystal chemistry of the ternary system SrO-Bi₂O₃-CuO as well as its boundary binary systems. A portion of the binary SrO-CuO system was previously published [16], and the structure of the compound "Sr₁₄Cu₂₄O₄₁" was determined [17]. Because of the relative importance of the phase Sr₂Bi₂CuO₆, a separate paper was prepared concerning the composition, unit cell dimensions and symmetry of this phase [18]. The experimental details, phase relations and crystal chemistry of the binary CaO-Bi₂O₃ and the two remaining ternary systems CaO-Bi₂O₃-CuO and SrO-CaO-Bi₂O₃ are reported in separate publications [19,20].

In the following discussion of phase equilibria and crystal chemistry, the oxides under consideration will always be given in the order of decreasing ionic radius, largest first, e.g., $SrO:\frac{1}{2}Bi_2O_3:CuO$. The notation $\frac{1}{2}Bi_2O_3$ is used so as to keep the metal ratios the same as the oxide ratios. The standard cement/ceramic notation is used for short hand with S=SrO, $B=\frac{1}{2}Bi_2O_3$ and C=CuO. Thus compositions may be listed simply by numerical ratio,

e.g., the formula $Sr_2Bi_2CuO_6$ can be written as S_2B_2C or simply 2:2:1.

2. Experimental Procedures

In general, about 3.5 g specimens of various compositions in binary and ternary combinations were prepared from SrCO₃, Bi₂O₃, and CuO. Neutron activation analyses of the starting materials indicated that the following impurities (in $\mu g/g$) were present: in CuO-3.9Cr, 2.8Ba, 28Fe, 410Zn, 0.09Co, 1.9Ag, 0.03Eu, 14Sb; in Bi_2 O₃-2.1Cr, 0.0002Sc, 26Fe, 21Zn, 0.6Co, 0.5Ag, 0.0008Eu, 0.2Sb; in $SrCO_3 - 320Ba$, 0.001Sc, 6.3Fe, 3.7Zn, 0.1Co, 0.002Eu. The constituent chemicals were weighed on an analytical balance to the nearest 0.0001 g and mixed either dry or with acetone in an agate mortar and pestle. The weighed specimen was pressed into a loose pellet in a stainless steel die and fired on an MgO single crystal plate, or on Au foil, or on a small sacrificial pellet of its own composition. The pellets were then calcined several times at various temperatures from ~600 °C to 850 °C, with grinding and repelletizing between each heat treatment. Duration of each heat treatment was generally about 16-20 h. For the final examination a small portion of the calcined specimen was refired at the desired temperature (1-8 times), generally overnight, either as a small pellet or in a small 3 mm diameter Au tube, either sealed or unsealed. Too many heat treatments in the Au tube generally resulted in noticeable loss of Cu to the Au vessel.

When phase relations involving partial melting were investigated, specimens were contained in 3 mm diameter Au, Pt or Ag/Pd tubes and heated in a vertical quench furnace. This furnace was heated by six MoSi₂ hairpin heating elements with vertical 4-in diameter ZrO₂ and 1-in diameter Al₂O₃ tubes acting as insulators. The temperature was measured separately from the controller at a point within approximately 1 cm of the specimen by a Pt/90Pt10Rh thermocouple, calibrated against the melting points of NaCl (800.5 °C) and Au (1063 °C). After the appropriate heat treatment the specimen was quenched by dropping it into a Ni crucible, which was cooled by He flowing through a copper tube immersed in liquid N₂.

In order to approach equilibrium phase boundaries by different synthesis routes, many specimens were prepared from pre-made compounds or two-phase mixtures as well as from end members. These were weighed, mixed and ground in the same way as for the previously described specimens. Also, some specimens were: 1) annealed at some temperature (T_1) and analyzed by x-ray powder diffraction; 2) annealed at a higher or lower temperature (T_2) where a different assemblage of phases was observed; and 3) returned to T_1 to demonstrate reversal of the reaction(s) between T_1 and T_2 . All experimental details are given in tables 1a and 1b. Phase identification was made by x-ray powder diffraction using a high angle diffractometer with the specimen packed into a 5 or 10 mil deep cavity in a glass slide. The diffractometer, equipped with a theta compensating slit and a graphite diffracted beam monochromator, was run at $\frac{1}{4}$ °2 θ /min with CuK α radiation at 40 KV and 30 MA. The radiation was detected by a scintillation counter and solid state amplifier and recorded on a chart with $1^{\circ}2\theta=1$ in. For purposes of illustration and publication, the diffraction patterns of selected specimens were collected on a computer-controlled, step scanning goniometer and the results plotted in the form presented.

Equilibrium in this system has proven to be so difficult to obtain that a few specimens were prepared by utilizing an organic precursor route to obtain more intimate mixtures at low temperatures. It is relatively simple to make mixtures of SrO (with or without CaO) and CuO by utilizing acetate solutions or acrylic acid, but Bi2O3 is not soluble in these solutions. The carbonates of all three (or four) oxides were therefore dissolved in lactic acid and dried by slow heating in a container with a large surface-to-volume ratio. This procedure yields an essentially single phase amorphous precursor for all compositions that contain less than about 66.7 mole percent Bi₂O₃. At higher bismuth contents, pure Bi metal was formed by carbothermic reduction under even the lowest temperature drying procedures in air.

3. Experimental Results and Discussion

Most of the experiments performed on the binary and ternary mixtures of SrO:Bi₂O₃:CuO are reported in table 1a. Additional experiments specifically designed in an attempt to obtain crystals large enough for x-ray single crystal study are detailed in table 1b. Crystallographic data for various phases are reported in table 2.

3.1 The System Bi₂O₃-CuO

A phase diagram for this system was already published [21], and was redrawn as figure 6392 in Phase Diagrams for Ceramists (PDFC) [22]. It apparently contains only one compound, Bi_2CuO_4 (B_2C), which is tetragonal, space group P4/ncc, a=8.510, c=5.814 Å [23]. The x-ray powder diffraction data for Bi_2CuO_4 were also reported in [23]. The very limited number of experiments performed during the course of this work, as shown in table 1, confirms that this is the only compound formed in the system. No attempt was made to reinvestigate the melting relations of this system because it does not have any great effect on the phase equilibria of the ternary system with SrO.

3.2 The System SrO-CuO

Phase equilibria in the high CuO portion of the system were shown in [16], where the new compound "Sr₁₄Cu₂₄O₄₁" (S₁₄C₂₄) was proven to exist along with the previously reported SrCuO₂ [24] and Sr₂CuO₃ [25]. Refined unit cell dimensions and standard x-ray powder diffraction data for the last two phases were recently reported: SrCuO₂ (SC) [26] is orthorhombic (Cmcm) with a = 3.5730(2), b = 16.3313(8), c = 3.9136(2) Å; Sr_2CuO_3 (JCPDS 34-283) is also orthorhombic (Immm) a = 3.4957, b = 12.684, c = 3.9064 Å. The unit cell dimensions of $Sr_{14}Cu_{24}O_{41}$ ($S_{14}C_{24}$) [16,17] indicate that it is face centered orthorhombic with a = 11.483(1), b = 13.399(1) and c = 3.9356(3) Å; there are also some superstructure peaks in the pattern which may possibly be indexed on an incommensurate cell that has a c-axis which is about 7 times that of the subcell. The partially indexed x-ray powder diffraction data is given in table 3 and the pattern is illustrated in figure 1.

Determinations of the melting relations in the high-SrO portion of the system were complicated by charge-capsule reactions (table 1). Specimens of SrCuO₂ and Sr₂CuO₃ (SC and S₂C) were calcined to single phase and then small portions reheated in 3-mm diameter unsealed Pt tubes; Au capsules could not be used because the melting points of interest were higher than that of Au (1063 °C). Even though these experiments had a maximum duration of no more than 10 min at high-temperature, some CuO always alloyed with the Pt even at

Table 1a. Experimental data for the ternary system SrO-Bi₂O₃-CuO

Spec.	Co	omposition, n	nole	Temperature of heatreatment; °C ^b	t Visual observation	Results of x-ray diffraction ^o
no.	SrO	$\frac{1}{2}$ Bi ₂ O ₃	CuO	Initial Final		,
	75.0	12.5	12.5	700 750 800 850		$SrCO_3+S_3B+"7:2:2"$ $S_3B+SrCO_3+S_2C+"7:2:2"_{tr}$ $S_3B+S_2C(+SrO?)$ $S_3B+S_2C(+SrO?)$
	65	10	25	700 750 800 850 900		$SrCO_3 + CuO + "7:2:2" + S_{14}C_{24} + S_3B_{tr} \\ "7:2:2" + S_2C + S_3B + CuO_{tr} \\ S_2C + S_3B + "7:2:2" \\ S_2C + SC + S_3B_{2tr} + "7:2:2"_{tr} \\$
	64.29 <i>SrCO</i> ₃ :5 1: 1 :	28.57 S ₂ C:S ₃ B ₂ 2	7.14	800×3 800×5		$S_3B+S_3B_2+$ "7:2:2" $S_3B+S_3B_2+$ "7:2:2"
#1 ^d	63.63	18.18	18.18	700 750 800 800×3 800×6 850		"7:2:2"+S ₃ B+S ₃ B ₂ +S ₂ C+SC+CuO "7:2:2"+S ₃ B+S ₃ B ₂ +SC+S ₂ C "7:2:2"+S ₃ B+S ₃ B ₂ +SC+S ₂ C S ₃ B ₂ +S ₂ C+"7:2:2"+SC+S ₃ B
#2	S₂C:S₃B 2:1	32		875× 875× 875×	2	$S_3B_2+S_2C+X(30.25^\circ)$ $S_3B_2+S_2C+X(30.25^\circ)$ $S_3B_2+S_2C+X(30.25^\circ)_{tr}$
#3	S₂C:S₃B 2:1	β_2		800×3 800×5 900×	3	$S_3B + S_3B_2 + "7:2:2" + S_2C + SC S_3B + "7:2:2" + SC + S_2C_{tr} + S_3B_{2tr} S_3B_2 + S_2C + S_3B_{tr} + X(30.25°)_{tr}$
#1	63.33 ¹ 2Bi ₂ O ₃ :S 1.00:6		31.67	750 850 900 950		$S_2C+SC+S_3B_2+X_{tr}$ $S_2C+SC+S_3B_2+X_{tr}$
#2	½Bi₂O₃:S 1.00:6			875×	5	$S_2C + SC + S_3B_2 + X$
#1	60 ½Bi ₂ O ₃ :S 1:3	10 5₂C	30	750 850 900 950		$S_2C+SC+S_3B_2+X_{tr} \\ S_2C+SC+S_3B_2+X_{tr}$
#2	½Bi ₂ O ₃ :S 1:3	S₂C		875×	5	$S_2C + SC + S_3B_2 + X$
#1	60	20	20	700 750 800 850 900 900×	3	"7:2:2"+S ₃ B+CuO+SrCO ₃ "7:2:2"+SC+S ₂ C SC+S ₂ C+unk(11")+"7:2:2" SC+S ₂ C+unk(11") S ₃ B ₂ +SC+S ₂ C

Table 1a. Experimental data for the ternary system SrO-Bi₂O₃-CuO—Continued

Cor		nole	Temperature	of heat	Visual	Results of
SrO	percent ^a ¹ 2Bi ₂ O ₃	CuO	treatment; Initial	°C° Final	observation	x-ray diffraction ^c
		·	700		 	
						"7:2:2" $+S_3B_2+SC+S_2C+S_3B+Cu^2$
						$"7:2:2" + S_3B_2 + SC + S_2C + S_3B$
			0227,10	800×6		"7:2:2" $+S_3B_2+SC+S_2C+S_3B$
				850		$S_3B_2+S_2C+SC+"7:2:2"$
$S_2C:S_2B_2$			700			
2:1			750			
						$S_3B_2 + SC + "7:2:2" + S_2C + S_3B$
			800×3			$S_3B_2+SC+"7:2:2"+S_2C+S_3B$
						"7:2:2" + S_3B_2 + SC + S_2C + S_3B
				850		$S_3B_2+S_2C+SC+"7:2:2"$
57 14	28.57	14.29	700			
57.11	20.57	11.25				
				875		$S_3B_2 + SC + 2:2:1_{tr}$
				900		$S_3B_2 + SC + 2:2:1_{tr}$
				900×3		$S_3B_2 + SC + 2:2:1_{tr}$
55	35	10				$S_3B_2+2:2:1+X$ $S_3B_2+2:2:1+X$
				900(Ag/Fu')		33B2+2:2:1+A
55	20	25				
				875		$SC + S_3B_2 + 8:4:5$
				875×2		$SC + S_3B_2 + 8:4:5$
				875×4		$SC + S_3B_2 + 8:4:5_{tr}$
		35	750			
_	CSC					
2:4:3			830	000		$SC+S_2C+S_3B_2$
						$SC+S_2C+S_3B_2$ $SC+S_2C+S_3B_2$
				750		30 320 33D2
$\frac{1}{2}Bi_{2}O_{3}:S_{2}$	C:SC			875×5		$SC+S_2C+S_3B_2+X$
2:4:3						
50	40	10	850			$S_3B_2+2:2:1$
30	70	10	830	875		$S_3B_2+2:2:1$ $S_3B_2+2:2:1$
						G ₃ D ₂ † 2.2.1
50	35	15	875			$S_3B_2+2:2:1$
				900		$S_3B_2+2:2:1+8:4:5+SC_{tr}$
				900-3days		$S_3B_2+2:2:1+3:2:2+8:4:5+SC$
				900×3		$S_3B_2+2:2:1+8:4:5+3:2:2+SC$
G D .CC	•		650			
1.100/:1.	0000					$2:2:1+S_3B_2+SC$
			800	975		$2:2:1+S_3B_2+SC$ $2:2:1+S_3B_2+SC$
				673		2.2.1 + 5312 + 50
50	25	25	700			
			750×2			$SrCO_3 + CuO + S_3B + S_{14}C_{24} + "7:2:2"$
				750×4(Au ^r)		$*+SC_{tr}+S_{14}C_{24tr}$
				800(Au¹)		$+8:4:5_{tr}+SC_{tr}+S_{14}C_{24tr}$
				$800\times2(Au^f)$		$+8:4:5_{tr}+SC_{tr}+S_{14}C_{24tr}$
				850(Au ^r)		8:4:5+*+SC _{tr}
				850×2(Au ^f)		$8:4:5+S_3B_2+SC$
				$850\times3(Au^f)$		$8:4:5+S_3B_2+SC$
				$880\times1(Au^f)$		$8:4:5+S_3B_2+SC$
				900(Au ^f)		$8:4:5+S_3B_2+SC$
	\$\frac{S_2C:S_2B_2}{2:1}\$ \$7.14 \$55 \$\frac{55}{2B_{12}O_3:S_2}\$ 2:4:3 \$50 \$50 \$\$50 \$\$50	SrO	SrO $\frac{1}{2}Bi_2O_3$ CuO $S_2C:S_2B_2$ 2:1 57.14 28.57 14.29 55 35 10 55 20 25 $SC:S_2B_2$ 2.5:1.0 35 $\frac{1}{2}Bi_2O_3:S_2C:SC$ 2:4:3 35 $\frac{1}{2}Bi_2O_3:S_2C:SC$ 2:4:3 10 50 35 15 $S_2B_2:SC$ 1.1667:1.0000	SrO $\frac{1}{2}Bi_2O_3$ CuO treatment; Initial 700 750 800 800×3 $S_2C:S_2B_2$ 700 750 800 800×3 800×3 800×3 57.14 28.57 14.29 700 55 20 25 $SC:S_3B_2$ 2.5:1.0 750 55 10 35 $\frac{1}{2}Bi_2O_3:S_2C:SC$ 750 2.4:3 850 $\frac{1}{2}Bi_2O_3:S_2C:SC$ 750 2.4:3 850 $S_2B_2:SC$ 650 1.1667:1.0000 750 800 800 50 25 25 700 750 800 800	SrO percent* ½Bi₂O₃ CuO treatment; ²Cb Initial Final 700 750 800 800×6 800 800×6 850 800 800×6 850 57.14 28.57 14.29 700 850 875 900 900×3 850 875 55 20 25 875(Ag/Pd¹) 55 20 25 875×4 55 10 35 875×2 2.51.0 875×2 875×4 55 10 35 875×2 2.4:3 850 900 2.4:3 850 900 50 35 15 875 50 35 15 875 50 25 25 700 750×2 750×4(Au¹) 800(Au¹) 850×3(Au¹) 850×2(Au¹) 850×3(Au¹) 875 875×5 875×5 875×5 875×5 875×5	SrO 1/2 Bi ₂ O ₃ CuO Initial Final Final

Table 1a. Experimental data for the ternary system SrO-Bi₂O₃-CuO-Continued

S	Cor	mposition, m	nole	Temperature		Visual	Results of
Spec. no.	SrO	percent ^a ½Bi ₂ O ₃	CuO	treatment Initial	Final	observation	x-ray diffraction ^c
±2	SC:S ₂ B ₂ 1.0:0.5			880×1 880×5 900×3			SC+2:2:1+S ₃ B ₂ 8:4:5+2:2:1+S ₃ B ₂ +SC 8:4:5+S ₃ B ₂ +SC
# 3				650 750 800			$S_3B_2 + SC + 2:2:1$
					875 900(Au ^t) 900×3(Au ^t) 900×6(Au _t) 925(Au ^t) 950(Au ^t)	part.melt	$SC+2:2:1+S_3B_2+8:4:5$ $SC+8:4:5+S_3B_2$ $SC+8:4:5+S_3B_2$ $SC+8:4:5+S_3B_2$ $SC+8:4:5+S_3B_2$ $SC+8:4:5+S_3B_2$ $SC+S_3B_2+Rav$
				950(Au ^t)	900(Au ¹) 875(Au ¹)		$SC+S_3B_2+8:4:5$ $SC+S_3B_2+8:4:5$
	50.00	16.50	33.50	650 750 800 850	875 900 900×3		$SrCO_3 + CuO + "7:2:2" + SC_{tr}$ $CuO + SC + "7:2:2" + S_{14}C_{24}$ $SC + S_3B_2 + 2:2:1 + S_2C$ $SC + S_3B_2 + 2:2:1$ $SC + S_3B_2 + 2:2:1 + 8:4:5$ $SC + S_3B_2 + 8:4:5$
[£] 1	48.75 SC:SB ₂ 18.5:1.0	5.00	46.25	750 850	900 950	sl. melting	SC+2:2:1+8:4:5 SC+Rav+S ₃ B _{2tr}
2	SC:SB ₂ 18.5:1.0				875×5		SC+8:4:5+X
1	47.5 SC:SB ₂ 8.5:1.0	10.0	42.5	750 850	900		SC+2:2:1+3:2:2+8:4:5 _{tr}
					950	part.melt	$SC+Rav+S_3B_{2tr}$
2	SC:SB ₂ 8.5:1.0				875×5		SC+8:4:5+3:2:2
1	47.06 (8:4:5)	23.53	29.41	700 750×2	800(Au ^f)		SrCO ₃ +CuO+Rav+unk(4.40°) SrCO ₃₊ CuO+Rav+unk(4.40°) +unk(4.80°)
				900(Au ^r)	850(Au ^f) 850×2(Au ^f) 875(Au ^f) 900(Au ^f)		unk(4.80°)+CuO+SrCO ₃ unk(4.80°)+CuO+SrCO ₃ 2:2:1+Rav+SC unk(4.40°)+unk(4.80°)+CuO

Table 1a. Experimental data for the ternary system SrO-Bi₂O₃-CuO—Continued

Spec.	Composition, mole percent ^a			Temperatur treatmen	e of heat	Visual observation	Results of x-ray diffraction ^c
no.	SrO	½Bi₂O₃	CuO	Initial	Final	Oosel vation	x-ray diffraction
#2				875	M		$S_3B_2+2:2:1+SC+S_{14}C_{24}+Rav$
							$+3:2:2+S_3B$
					900		$S_3B_2 + SC + 2:2:1 + 3:2:2 + 8:4:5$
					900×2		$S_3B_2 + SC + 2:2:1 + 3:2:2 + 8:4:5$
					950	part.melt	$S_3B_2+Rav+SC$
// -							7.5.5.50
#3L8				650 750			$B_2C+SrCO_3+CuO$
				850			$2:2:1+S_3B_2+SC+3:2:2+S_{14}C_{24}$
					850×2		$2:2:1+S_3B_2+SC+3:2:2+S_{14}C_{24}$
				450			
				850×2			
					900×1		8:4:5+2:2:1+SC
					900×4		8:4:5+2:2:1+SC _{tr}
					925		$8:4:5+SC_{tr}$
#4				850			
F- -				1250 ^h		comp.melt	
					900(0 ₂ i)	•	8:4:5
					$925(0_2^{i})$		8:4:5
					(-2)		
‡ 1	45	20	35	850			
				875	055.45		55 + 300 + 5 - 5
					875×7		$SC + 3:2:2 + S_{14}Cu_{24}$
					900		$SC + Rav + S_3B_2 + 8:4:5$
					900×3		SC+3:2:2
# 2				875			
					900		3:2:2+SC+2:2:1
#3	$SC:SB_2$			800			
₁ - 5	3.5:1.0			875×1			$SC+S_{14}C_{24tr}$
	3.3.1.0			0/5/(1	875×6		SC+2:2:1+8:4:5
					0/5/(0		50 2.2.1 + 0.4.5
	45	45	10	700			
				800			
				850	875		$S_2B_2 + 2:2:1$
					073		$S_2 D_2 + 2.2.1$
	45	35	20	700			
				800			
				850			
					875		$2:2:1+S_3B_2+SC$
	44.44	22.22	22.22	700	900		$2:2:1+S_3B_2+SC$
	44.44	33.33	22.22	700 850			$2:2:1+S_3B_2+SC+S_{14}C_{24}$
				875			$2:2:1+S_3B_2+SC+S_{14}C_{24}$ $2:2:1+S_3B_2+SC+S_{14}C_{24}+3:2:2$
				= -	900		$2:2:1+S_3B_2+8:4:5+3:2:2+SC_{tr}$
					900×3		S_3B_2+Rav
	44	36	20	700			
				800			
				850			
				850	875		$2:2:1+S_3B_2+SC$

Table 1a. Experimental data for the ternary system SrO-Bi₂O₃-CuO-Continued

Spec.	Co	mposition, n	ıole	Temperature treatment;		Visual observation	Results of x-ray diffraction ^c
no.	SrO	¹ / ₂ Bi ₂ O ₃	CuO	Initial	Final	Obbot varion	n ray diffiaction
	43.75	25.00	31.25	700			
				750			
				850	926		222 - CO - C - C - C - C
					875 900		$3:2:2+SC+S_{14}C_{24}+S_3B_2$
					900×2		$3:2:2+SC+S_{14}C_{24}+2:2:1_{tr}$ $3:2:2+SC+S_{14}C_{24tr}$
					300 X 2		3:2:2+3C+314C24tr
	43.62	32.98	23.40	700			
				750			
				850			
					875		$2:2:1+3:2:2+S_{14}C_{24}+SC$
					900		$2:2:1+3:2:2+SC+8:4:5_{tr}$
	43	37	20	700			
	10			800			
				850			
					875		$2:2:1+SC+S_3B_2$
					900		$2:2:1+SC+S_3B_2$
	42.86	32.65	24.49	700			
	42.00	32.03	24.47	750 750			
				850			
					875		$2:2:1+3:2:2+S_{14}C_{24}+SC$
					900		$2:2:1+3:2:2+S_{14}C_{24}+SC$
	42.06	20.57	20.57	700			
1	42.86 (3:2:2)	28.57	28.57	850			
	(3.2.2)			875			$2:2:1+SC+S_{14}C_{24}+3:2:2+S_{3}B_{2t_{1}}$
				•	900×3(Auf)		$2:2:1+SC+8:4:5+3:2:2+S_3B_{2tr}$
					900×6(Au ^f)		$2:2:1+8:4:5+S_3B_2$
					900×8(Au')		$2:2:1+8:4:5+S_3B_2$
2				700			
2				750			
				850			
				875			$2:2:1+SC+S_{14}C_{24}+3:2:2+S_3B_2$
					900		$3:2:2+SC_{tr}+S_{14}C_{24tr}$
					900×2		$3:2:2+SC_{tr}+S_{14}C_{24tr}$
					925(O ₂ i)		$3:2:2+S_{14}C_{24tr}$
					925×2(O₂i)		3:2:2+S ₁₄ C _{24tr}
					950(O ₂ i)	part.melt	Rav+8:4:5+SC
3L ^g					900×2		2:2:1+3:2:2+SC
					900×3		2:2:1+3:2:2+SC
	40.5	47 E	10	P00			S ₂ B ₂ +Rav
	42.5	47.5	10	800	875		$S_2B_2 + Rav$ 2:2:1+ $S_2B_2 + Tet$
					925	comp.melt	Rav + Tet
						-	-
	42.16	32,35	25.49	700			
				750			
				850	875		$2:2:1+3:2:2+S_{14}C_{24}+SC$
					900		$2:2:1+3:2:2+S_{14}C_{24tr}+SC_{tr}$ $2:2:1+3:2:2+S_{14}C_{24tr}+SC_{tr}$
					- 00		
	42	40	18	700			
				850			
					875		$2:2:1+S_3B_2+S_{14}C_{24tr}$

Table 1a. Experimental data for the ternary system SrO-Bi₂O₃-CuO—Continued

ec.	Co	mposition, n	nole		Temperature of heat treatment; °C ^b		Results of x-ray diffraction ^c
0.	SrO	$\frac{1}{2}$ Bi ₂ O ₃	CuO	Initial	Final	observation	
	42	41	17	700			
				850			
					875		$2:2:1+S_3B_2+S_2B_2$
	42	38	20	700			
				800			
				850			
					875 900		$2:1:1+S_{14}C_{24}+SC$
					900		2:2:1+SC
	41.67	33.33	25.00	700			
				750			
				850	075		221.00.0.1221.00
					875 900		$2:2:1+S_{14}C_{24}+3:2:2+SC_{tr}$ $2:2:1+3:2:2+S_{14}C_{24tr}$
					900×2		$2:2:1+3:2:2+S_{14}C_{24tr}$ $2:2:1+3:2:2+S_{14}C_{24tr}$
					900(O ₂ i)		$2:2:1+3:2:2+S_{14}C_{24}^{j}$
					925(Au ^t)	part.melt	Rav+SC _{tr}
			•		925(O ₂ i)	no melting	$2:2:1+3:2:2+S_{14}C_{24}$
	41	44	15	700			
	71		**	850			
					875		$2:2:1+Rav+S_2B_2$
					900		$2:2:1+S_2B_2+Rav$
	41	43	16	700			
	7.		••	850			
					875		$2:2:1+S_2B_2+Rav$
					900		$2:2:1+S_2B_2$
	41	42	17	700			
				850			
					875		$2:2:1+S_2B_2$
					900		$2:2:1+S_2B_{2tr}$
	41	41	18	700			
				850			
					870		$2:2:1+S_3B_{2tr}$
					900 925	part.melt	$2:2:1+S_{14}C_{24tr}$ 2:2:1+Rav
					889k	part.men	2:2:1+Rav Rav+2:2:1
							=
	41	40	19	700			
				850	0=0		2:2:1
					870 900		$2:2:1+S_{14}C_{24tr}$ $2:2:1+S_{14}C_{24tr}$
					900(Au ^f)Q		$2:2:1+S_{14}C_{24tr}$ 2:2:1+Rav
					,, , , 		;·
	41	39	20	700			
				800			
				850	875		$2:2:1+S_{14}C_{24}$
					900		$2:2:1+S_{14}C_{24}$ $2:2:1+S_{14}C_{24}$

Table 1a. Experimental data for the ternary system SrO-Bi₂O₃-CuO-Continued

	Co	mposition, n	ıole	Temperature		Visual	Results of	
pec. no.	SrO	percent ^a ½Bi ₂ O ₃	CuO	treatment; Initial	°C ⁶ Final	observation	x-ray diffraction ^c	
	40.67	40.32	19.00		,			
	S•B•S ₂ B			990			2.2.1 + Boy	
	1.00:0.4	5:1.00		880	880×5		2:2:1+Rav	
							2:2:1 + Ray	
					900		2:2:1 + Rav	
	40.5	49.5	10.0	750			$S_2B_2+SB_2+Rav$	
	40.5	47.5	10.0	800			$Rav + S_2B_2 + Tet$	
				850			$Rav + S_2B_2 + Tet$	
					875		Tet + Rav + 2:2:1	
	40.5	40.5	19.0	700				
				850				
					870		$2:2:1+S_{14}C_{24tr}$	
					900		$2:2:1+S_{14}C_{24tr}+Rav_{tr}$	
				925				
					889 ^k	part.melt	2:2:1+Rav	
	40	41	19	700				
				850	070		001 · B	
					870		2:2:1+Rav	
					900		$2:2:1+Rav_{tr}$	
1	40	40	20	650				
1	70	40	40	750			$Rav + S_2B_2$	
				800			$2:2:1+S_2B_2+Rav$	
				000	850		$2:2:1+S_{14}C_{24tr}+Rav_{tr}$	
					870		$2:2:1+S_{14}C_{24tr}+Rav_{tr}$	
					900		$2:2:1+S_{14}C_{24ir}+Rav_{ir}$	
2				650				
				750				
				800				
				850				
				870				
					900		$2:2:1+S_{14}C_{24tr}+Rav_{tr}$	
					900(Au ^f)Q		2:2:1+Rav	
•	CC.CD							
3	<i>SC:SB₂</i> 1:1				850×1		$Rav + SC + 2:2:1 + SB_{2tr} + S_2B_{2tr}$	
	1.1				850×2		$2:2:1 + Rav + SC_{tr} + S_{14}C_{24tr}$	
					555/(2			
4	$SC:SB_2$							
	1:1			650				
				750				
				800				
					875		$2:2:1+Rav+S_{14}C_{24tr}$	
					925		$2:2:1+Rav+S_{14}C_{24tr}$	
5	S_2B_2 :Cue	0						
	1:1			880			Rav+2:2:1	
				880×5			2:2:1+Rav	
					900(0 ₂ i)		Rav +2:2:1	
					950	comp.melt	001.7	
					875		2:2:1+Rav ¹	
					$900-PO_2 = 0.15^{m}$		2:2:1+Rav ^m	

Table 1a. Experimental data for the ternary system SrO-Bi₂O₃-CuO—Continued

_	Composition, mole percent ^a			Temperature of heat treatment; °C ^b		Visual	Results of
c.	SrO	percent ^a ¹ / ₂ Bi ₂ O ₃	CuO	Initial	Final	observation	x-ray diffraction ^c
				800(O ₂ i)			
				$850(O_2^i)$			Rav+2:2:1
				(-/	900(O ₂ i)		Rav+2:2:1
				850			
				1250 ^h		comp.melt	$Rav + S_3B_2$
					800	•	$Rav + 2:2:1_{tr}$
					850		$Rav + 2:2:1_{tr}^{n}$
					900		$Rav + 2:2:1^n$
					900×2		Rav+2:2:1 ⁿ
					900×3		Rav + 2:2:1
					900(O ₂ i)		Rav
					$925(O_2^i)$		Rav
	40	20	40	650			
				750			
				800			$Rav + 2:2:1 + CuO + S_2B_2 + X$
					850		$2:2:1+S_{14}C_{24}+SC$
					900		$2:2:1+3:2:2+S_{14}C_{24}+SC_{tr}$
				650			
				750			
					900(Au ^f)		$Rav + SC + S_2B_2 + S_{14}C_{24}$
					900×3(Au ^f)		8:4:5+SC+Rav
					950		$Rav + SC + S_2B_2 + X$
	38	42	20				
	S2B2:Tet						
		.45:1.00			880×1		Rav+2:2:1
					880×5		Rav +2:2:1
	37	44	19	700			
	3,	• •	• >	850			
					900		Rav+2:2:1
	27	42	20	700			
	37	43	20	700 850			
				020	900		Rav+2:2:1
					870		Rav+2:2:1
							•
	36.66	53.33	10.00	700			n
				750			$Rav + SB_2 + S_2B_2$
				850	0.75		$Rav + SB_2 + Tet$
					875	part.melt	$Rav + SB_2 + Tet$
	36.66	36.66	26.66	650			
				750			$Rav + S_2B_2 + CuO$
				800			$Rav + 2:2:1 + CuO + S_{14}C_{24}$
				850			$2:2:1+Rav+CuO+S_{14}C_{24}$
					870		$2:2:1+Rav+CuO+S_{14}C_{24}$
					900		$2:2:1+Rav+CuO+S_{14}C_{24}$
	36.15	44.50	19.35				
			-,,,,,,				
	S.B Ri	5O:SC					
	S•B• ¹ ₂ Bi 0.7000:1	.4444:1.0000		880			Rav

Table 1a. Experimental data for the ternary system SrO-Bi₂O₃-CuO—Continued

Spec.	Con	nposition, m percent ^a	iole	Temperature treatment;	of heat	Visual observation	Results of x-ray diffraction ^c
no.	SrO	¹ ₂ Bi ₂ O ₃	CuO	Initial	Final	oosei vanon	x-ray diffraction
	36	45	19	700			
				850			
					900		Rav+2:2:1
#1	36	44	20	700			
•				750			$Rav + S_2B_2 + SB_2$
				875×7			Rav
					880(Au ^t)		Rav
					880×2(Auf)		Rav
					900×3		Rav
#2	Tet:CuO			800			
,, 2	9:5				875		Rav
					875×5		Rav
#3	Rhomb:S	C		875×5			Rav+2:2:1
	1.00:1.			,,-		950	comp.melt
		•			875		Rav+2:2:1
	25.00	42.14	21.57	900			
	35.29 <i>Tet:CuO</i>	43.14	21.57	800 875			Rav+CuO
	9.0:5.5			013	875×5		Rav+CuO
	7.0:3.3				013/2		May Tou
	35	48	17	700			
				850			
					875		Rav+Rhomb _{tr}
	35	47	18	700			
				850			
					875		$Rav + Rhomb_{tr}$
	35	46	19	700			
	33	40	19	850			
					875		Rav+Rhomb
	25	45	20	700			
	35	45	20	700 850			
				875			Rav
					900×3(Au')		Rav
	25	5	60	700			
	35	5	60	700 850			
					900		$S_{14}C_{24}+Rav+CuO$
	34.66	55.33	10.00	700 750			
				750			CD . D
				800			SB ₂ +Rav
				850	07 <i>E</i>	mont m -1+	SB ₂ +Rav
					875	part.melt	SB_2+Rav
	34	47	19	700			
				800			_
					875		Rav

Table 1a. Experimental data for the ternary system SrO-Bi₂O₃-CuO—Continued

Spec.	Co	mposition, m percent ^a	ole	Temperature treatment;		Visual observation	Results of x-ray diffraction ^c
no.	SrO	¹ ₂ Bi ₂ O ₃	CuO	Initial	Final	Josef varion	A-14y GHII4CHOH
	34	46	20				
	$\frac{1}{2}Bi_2O_3$: T	et:SC					
	1.4444:0	.7:1.0		880			Rav
				880×1			Rav
				880×2			Rav
				880×5			Rav
				990 X 3	000		
					900	part.melt	Rav
					1000	comp.melt	Rav
#1	33.33	33.33	33.33	800(12hr)			
					900(2hr) ^p		$Rav + CuO + 2:2:1 + S_{14}C_{24}$
‡ 2				650			
				750			$Rav + CuO + S_{14}C_{24}$
				800			$Rav + CuO + S_{14}C_{24} + 2:2:1_{tr}$
				850			$Rav + CuO + 2:2:1 + S_{14}C_{24}$
					870		$Rav + CuO + 2:2:1 + S_{14}C_{24}$
					900		$Rav + CuO + 2:2:1 + S_{14}C_{24}$ $Rav + CuO + 2:2:1 + S_{14}C_{24}$
					700		Ray TCUO T 2:2:1 + 314C24
# 3	¹ ₂ Bi ₂ O ₃ :S	C		800	i		$Rav + SC + CuO + S_{14}C_{24}$
	1:1			850			$Rav + CuO + S_{14}C_{24}$
# 4	^I ₂ Bi ₂ O ₃ :S	C		650			
	1:1			750			
				800			
					875		$Rav + S_{14}C_{24} + CuO$
					900×3(Au ^f)		$2:2:1+Rav+S_{14}C_{24tr}$
					,		
	33	47	20	700 850			
				050	875		Rav
	32	48	20				
			20				
	$\frac{1}{2}Bi_2O_3:T$			000: -4			n . nt . t
	1.6667:0	.6000:1.0000		880×1			Rav+Rhomb _{tr}
				880×5			Rav+Rhomb
	32	46	22				
	$\frac{1}{2}Bi_2O_3:T$	et:SC					
	1.5353:0	.4545:1.0		880×2			Rav+CuO
				880×5			Rav+CuO
	31.842	5.000	63.158	700			
				850			
					900		$S_{14}C_{24}+Rav+CuO$
					700		514C24 T 1.GV T CUO
	31.33	58.66	10.00	700 750			
				750	0.50		D1 1 D
					850		Rhomb+Rav
					875	comp.melt	Rhomb+Rav
#1	30.75	47.25	22.00				
	$\frac{1}{2}Bi_2O_3:T$			750			
		.3977:1.0		850			
	1.5015.0				900	Slight melt	Rav+Rhomb
					700	ongue men	1994 - Limonio

Table 1a. Experimental data for the ternary system SrO-Bi₂O₃-CuO-Continued

	Co	omposition, m	ole	Temperatu		Visual	Results of
Spec.		percenta		treatmen		observation	x-ray diffraction ^c
no.	SrO	$\frac{1}{2}$ Bi ₂ O ₃	CuO	Initial	Final		
#2			-	700			
				850			
					875		Rav
	30	50	20				
	$\frac{1}{2}Bi_{2}O_{3}$; T_{2}	Tet:SC					
	1.8888:0	0.5000:1.0000		880			Rav + Rhomb
					880×5		Rav+Rhomb
	30	47	23				
	$\frac{1}{2}Bi_{2}O_{3}:T_{2}$	Tet:SC					
	1.6715:0	0.3043:1.0000		880×2			Rav+CuO+Rhomb
				880×5			Rav+CuO+Rhomb
	30	45	25				
	$\frac{1}{2}Bi_2O_3$: T	Tet:SC					
	1.5555:0	0.2000:1.0000		880×2			Rav+CuO
					880×5		Rav+CuO
	28	48	24				
	SrCO ₃ -	Bi₂O₃:Tet		880×2			$Rhom + Rav + CuO_{tr}$
		.7963:0.1667		880×5			Rhom+Rav+CuO _{tr}
	20.0	46.5	33.5	650			
				750			
					800		Rav+Rhomb+CuO
					850	consid.melt	$Rav + Rhomb + CuO_{tr}$
	10.00	56.66	33.33	700			
				750			Rhomb+B ₂ C+CuO
					800		$Rhomb + B_2C + CuO$

^a Starting materials: $SrCO_3$, Bi_2O_3 , CuO, except when listed in italics. Compositions given in italics were formulated from the listed prereacted compounds or compositions. $S_*B_* = Sr_{1.2407}Bi_{1.2222}O_{3.074}$, Rhomb= $SrBi_{2.75}O_{5.125}$, $Tet = SrBi_{1.22}O_{2.83}$.

⁵ Specimens were given all previous heat treatments listed in the initial column, sequentially, and held at temperature 16-24 h, with grinding in-between, for the number of times shown and then reheated at the final temperature overnight. Specimens were heated as pellets on Au foil or MgO single crystal plates, except as indicated. In general, only a small portion of the specimen used for the initial (calcined) heat treatments was used to make sequential "final" heat treatments. Q=quenched.

^c Compounds are listed in order of estimated amounts, most prevalent first.

tr=trace, just barely discernible

 $B_2C = Bi_2CuO_4$

 $S_2C = Sr_2CuO_3$

 $SC = SrCuO_2$

 $S_{14}C_{24} = Sr_{14}Cu_{24}O_{41}$

Rhomb=rhombohedral solid solution

 $SB_2 = SrBi_2O_4$

Tet=Tetragonal solid solution near SrBi_{1,22}O_{2,83}

 $S_2B_2 = Sr_2Bi_2O_5$

 $S_3B_2 = Sr_3Bi_2O_6$

 $S_3B = Sr_6Bi_2O_9$

 $^{2:2:1 =} Sr_2Bi_2CuO_6$

Rav=Raveau-type solid solution, ~Sr_{1.8-x}Bi_{2.2+x}CuO_z

 $^{8:4:5 =} Sr_8Bi_4Cu_5O_{19+x}$

 $^{3:2:2 =} Sr_3Bi_2Cu_2O_8$

X,unk=phases of unknown composition

[&]quot;7:2:2" = unknown phase, probably oxycarbonate with diffraction peaks a ~18.40° and ~21.27° 20

^{*=}unknown phase, probably an oxycarbonate, with diffraction peaks a 4.40° and 5.68° plus major peaks at 30.50° and 32.45° 20°

Footnotes to table 1a-Continued

Table 1b. Experimental conditions for crystal growth experiments

Charge	Flux	Container	Temperature cycle	Results
SrO:1/2Bi ₂ O ₃ 4:1	(KNa)C1	sealed small	800 °C 16 h	
98 wt%	2 wt%	diameter Au		
SrO:1/2Bi ₂ O ₃ 4:1	(KNa)Cl	sealed small diameter Au	800 °C 16 h	
90 wt%	10 wt%			
SrO:1/2Bi ₂ O ₃ 4:1	(KNa)Cl	sealed small diameter Au	1025→650 °C @ 5 °C/h	
80 wt%	20 wt%		@ <i>5</i>	
Sr ₆ Bi ₂ O ₉		open small diameter Au	925→900 °C @ 0.3 °C/h	
Sr ₆ Bi ₂ O ₉ 98 wt%	(KNa)Cl 2 wt%	sealed small diameter Au	900 °C 16 h	
Sr ₆ Bi ₂ O ₉ 98 wt%	(KNa)Cl 2 wt%	sealed small diameter Au	800 °C 16 h	
Sr ₆ Bi ₂ O ₉ 90 wt%	(KNa)C1 10 wt%	sealed small diameter Au	800 °C 16 h	S₃B oxychloride
Sr ₆ Bi ₂ O ₉ 80 wt%	(KNa)C1 20 wt%	sealed small diameter Au	1025→650 °C @ 5 °C/hr	S ₃ B ₂ xtls hydrate after long exposure to air
Sr ₆ Bi ₂ O ₉ 80 wt%	(KNa)C1 20 wt%	sealed small diameter Au	950→650 °C @ 4 °C/h	
SrO:1/2Bi ₂ O ₃ 2:1	(KNa)Cl	sealed small diameter Au	800 °C 16 h	
98 wt%	2 wt%			
SrO:1/2Bi ₂ O ₃ 2:1	(KNa)Cl	sealed small diameter Au	800 °C 16 h	
90 wt%	10 wt%			
$\mathrm{Sr}_2\mathrm{Bi}_2\mathrm{O}_5$		sealed small diameter Pt	925 °C 162 h	S_2B_2 Partially melted

^d These specimens are numbered when more than one batch of a given oxide ratio were prepared.

^c Specimens were heated in 70Ag/30Pd tubes, which caused the appearance of unknown phases due to reaction with the tube.

^f Specimens were contained in 3-mm diameter Au tubes. Excessive heat treatment in such tubes resulted in appreciable loss of Cu to the surrounding Au tube.

g L=Specimen prepared by an organic precursor route utilizing lactic acid.

^h The specimen was melted in an Al₂O₃ crucible and poured onto an Al chill plate.

i Specimen heated in one atmosphere pure oxygen instead of in air.

^j Increase in amount of S₁₄C₂₄ relative to 3:2:2; indicates that the 3:2:2 phase is not favored by higher oxygen partial pressure.

^k Specimen cooled from 925 to 889 °C at 1 °C/h.

¹ Amount of 2:2:1 phase not increased.

^m Specimen heated in atmosphere of mixed Argon/Oxygen with the partial pressure of oxygen equal to 0.15 atm; amount of 2:2:1 phase greatly increased.

ⁿ Amount of 2:2:1 phase increased relative to previous heat treatment.

^p This specimen was prepared as described in reference [30].

Table 1b. Experimental conditions for crystal growth experiments—Continued

Charge	Flux	Container	Temperature cycle	Results
Sr ₂ Bi ₂ O ₅		sealed small diameter Au	1025→950 °C @ 1 °/h	b.c. Tet
$Sr_2Bi_2O_5$		sealed small diameter Au	1025→900 °C @ 1 °C/h	b.c. Tet
Sr ₂ Bi ₂ O ₅		sealed small diameter Au	1025→900 °C @ 1 °/h; 875 °C-225 h	S_2B_2
Sr ₂ Bi ₂ O ₅ 98 wt%	(KNa)Cl 2 wt%	sealed small diameter Au	900→640 °C @ 3 °C/h	S_2B_2
Sr ₂ Bi ₂ O ₅ 90 wt%	(KNa)Cl 10 wt%	sealed small diameter Au	900→640 °C @ 3 °C/h	S_2B_2
Sr₂Bi₂O₅ 80 wt%	(KNa)Cl 20 wt%	sealed small diameter Au	900→640 °C @ 3 °C/h	
Sr ₂ Bi ₂ O ₅ 50 wt%	(KNa)Cl 50 wt%	sealed small diameter Au	900→640 °C @ 3 °C/h	
SrBi ₂ O ₄ 80 wt%	(KNa)Cl 20 wt%	sealed large diameter Au	900→850 °C @ 3 °C/h	
SrBi ₂ O ₄ 80 wt%	(KNa)Cl 20 wt%	sealed large diameter Au	900→700 °C @ 3 °C/h	
SrBi ₂ O ₄ 20 wt%	(KNa)Cl 80 wt%	sealed small diameter Au	800→645 °C @ 1 °C/h	SB ₂
SrBi ₂ O₄ 50 wt%	(KNa)Cl 50 wt%	sealed small diameter Au	800→645 °C @ 1 °C/h	SB ₂
SrBi₂O₄ 20 wt%	(KNa)Cl 80 wt%	sealed Pt	740→570°C @ 6°C/h	SB ₂
SrO:1/2Bi ₂ O ₃ :CuO 3:1:1 90 wt%	(KNa)Cl 10 wt%	sealed small diameter Au	900°C 16 h	xtals soluble in H₂O
SrO:1/2Bi ₂ O ₃ :CuO 2:1:1		large diameter Pt	950→615 °C @ 1 °C/min	
SrO:1/2Bi ₂ O ₃ :CuO 2:1:1 90 wt%	(KNa)Cl 10 wt%	sealed small diameter Au	900°C 16 h	
SrO:1/2Bi ₂ O ₃ :CuO 2:1:1 90 wt%	(KNa)Cl	sealed small diameter Au	900→650 °C @ 3 °C/h	partially melted needlelike xtals of 8:4:5
SrO:1/2Bi ₂ O ₃ :CuO 2:1:1 90 wt%	2NaF:SrF ₂ 50.86:49.14 10 wt%	sealed small diameter Au	900→650 °C 3 °C/h	Partially melted Rav
SrO:1/2Bi ₂ O ₃ :CuO 45:45:10		Ag/Pd small diameter tube	950→800 °C @ 1 °C/h	

Table 1b. Experimental conditions for crystal growth experiments—Continued

Charge	Flux	Container	Temperature cycle	Results
Sr ₃ Bi ₂ Cu ₂ O ₈ 90 wt%	(KNa)C1 10 wt%	sealed small diameter Au	900 °C 16 h	xtals not soluble in H₂O
SrO:1/2Bi ₂ O ₃ :CuO 42.5:47.5:10		Ag/Pd small diameter tube	950→800 °C @ 1 °C/h	
SrO:1/2Bi ₂ O ₃ :CuO 41:41:18		sealed small diameter Au	925→900°C @ 1°C/h	
SrO:1/2Bi ₂ O ₃ :CuO 41:40:19		open small diameter Au	900→450 °C @ 1 °C/h	
SrO:1/2Bi ₂ O ₃ :CuO 40.5:49.5:10		Ag/Pd small diameter tube	950→800°C @ 1°C/h	
SrO:1/2Bi ₂ O ₃ ;CuO 40.5:40.5:19		sealed small diameter Au	925→900 °C @ 1 °C/h	2:2:1+ Rav
Sr ₂ Bi ₂ CuO ₆		Ag/Pd small diameter tube	950→800 °C @ 1 °C/h	Rav+Tet
$Sr_2Bi_2CuO_6$		Pt small diameter tube	950→800 °C @ 1 °C/h	
$Sr_2Bi_2CuO_6$		sealed small diameter Au	950→800°C @ 1°C/h	Rav
$Sr_2Bi_2CuO_6$		open small diameter Au	950→400°C @ 1°C/h	
Sr ₂ Bi ₂ CuO ₆ 90 wt%	(KNa)C1 10 wt%	sealed small diameter Au	900 °C 16 h	Rav completely melted
Sr ₂ Bi ₂ CuO ₆	NaF:KF 42:58	sealed small diameter Au	900°C 3 d	Rav
98 wt%	2 wt%			
Sr ₂ Bi ₂ CuO ₆ 90 wt%	NaF:KF 42:58 10 wt %	sealed small diameter Au	900→650 °C @ 3 °C/h	Rav
		sealed small	850→650 °C	Rav
Sr ₂ Bi ₂ CuO ₆ 90 wt%	2NaF:SrF ₂ 50.86:49.14 10 wt%	diameter Au	@ 3 °C/h	Kav
Sr ₂ Bi ₂ CuO ₆	2NaF:CaF ₂ 51.73:48.28	sealed small diameter Au	900→650 °C 3 °C/h	Rav
90 wt%	10 wt%			
SrO:1/2Bi ₂ O ₃ :CuO 3:2:3	(KNa)Cl	sealed small diameter Au	1025→650 °C @ 5 °C/min	
80 wt%	20 wt%			
SrO:1/2Bi ₂ O ₃ :CuO 36:44:20 Rav		Ag/Pd small diameter tube	950→800 °C @ 1 °C/h	
SrO:1/2Bi ₂ O ₃ :CuO 1:1:1		large diameter Pt	950→615 °C @ 1 °C/min	
SrO:1/2Bi ₂ O ₃ :CuO 1:1:1	(KNa)Cl	sealed small diameter Au	1025→650 °C @ 5 °C/min	

Table 2. Crystallographic data

Phase		Unit cell par	ameters (Å)		Symmetry	Space	Reference
formula	a	b	c	β°		group	
Bi ₂ CuO ₄	8.510		5.814		Tet	P4/ncc	23
SrCuO ₂	3.5730(2)	16.3313(8)	3.9136(2)		Orth	Cmcm	26
Sr ₂ CuO ₃	3.4957	12.684	3.9064		Orth	Immm	JCPDS ^a 34-283
$Sr_{14}Cu_{24}O_{41}$	11.483(1)	13.399(1)	3.9356(3) ^b		Orth	Fmmm	This work
~Rhomb-SS° $Sr_xBi_{1-x}O_{(3-x)/2}$ $0.1 \le x \le 0.265$	3.979		28.51		Rhomb		27 ^d
SrBi ₂ O ₄	19.301(2)	4.3563(5)	6.1049(7)	94.85(1)	Mon	C2/m	This work
~ Tet-SS SrBi _{1.22} O _{2.83}	13.239(2)		4.257(1)		Tet	I4/m	27
$Sr_2Bi_2O_5$	3.8262(2)	14.307(1)	6.1713(4)		Orth	Cmcm	This work
$Sr_3Bi_2O_6$	12.526(1)		18.331(2)		Rhomb	R3m	This work
Sr ₆ Bi ₂ O ₉	6.009		58.663		Rhomb ^e		This work
Sr ₂ Bi ₂ CuO ₆	24.493(2)	5.4223(5)	21.959(2)	105.40(1)	Mon	C2/m	18
Raveau-SS $Sr_{1.8-x}Bi_{2.2+x}Cu_{1\pm x/2}O_z$ $0 \le x \le 0.15$	26.889(9)	5.384(2)	26.933(8)	113.67(3)	Mon	C2	This work ^f
$Sr_8Bi_4Cu_5O_{19+x}$	33.991(3)	24.095(2)	5.3677(5)		Orth	Fmmm	This work
$Sr_3Bi_2Cu_2O_8$	24.937(7)	5.395(2)	19.094(7)	96.97(3)	Mon	C2/m	This work

^a Joint Committee for Powder Diffraction Standards, X-Ray Diffraction card file.

temperatures well below melting. Partial melting was assumed to have occurred when the x-ray powder diffraction pattern of a quenched specimen indicated an abrupt change in the phase fraction of a second phase. Both SrCuO₂ and Sr₂CuO₃ melt incongruently: SrCuO₂ melts to liquid plus Sr₂CuO₃ at ~1085 °C, and Sr₂CuO₃ melts to liquid plus SrO, at ~1225 °C. The phase equilibria diagram constructed from the data in table 1 and the previously reported experiments [16] is shown in figure 2.

3.3 The System SrO-Bi₂O₃

The phase equilibria diagram for the system SrO-Bi₂O₃ was reported in [27] and redrawn as figure 6428 in PDFC [22] and figure 3 (where the scale is changed to $\frac{1}{2}$ Bi₂O₃:CuO instead of the original Bi₂O₃:CuO, to be consistent with the other phase diagrams in this report). Considerable effort was made to study the phase relations of this binary. Complete experimental results are published in [28], and the results are shown in figures 4a and 4b

^b Contains superstructure with c'=7c.

c -SS=solid solution.

d Unit cell dimensions for x=0.19.

^e Apparently a subcell.

f Unit cell dimensions for x=0.

Table 3. X-ray powder diffraction data for Sr₁₄Cu₂₄O₄₁

6.68 5.72 4.352 3.596 3.347 3.021 ^b 2.8879 2.8608 2.6853 2.6339 2.6049 ^b	2 <1 2 6 12	13.25 15.48 20.39 24.74 26.61	13.22 15.45 20.38	020 200
4.352 3.596 3.347 3.021 ^b 2.8879 2.8608 2.6853 2.6339 2.6049 ^b	2 6 12 1	20.39 24.74	20.38	
3.596 3.347 3.021 ^b 2.8879 2.8608 2.6853 2.6339 2.6049 ^b	6 12 1	24.74		
3.347 3.021 ^b 2.8879 2.8608 2.6853 2.6339 2.6049 ^b	12 1		04.55	220
3.021 ^b 2.8879 2.8608 2.6853 2.6339 2.6049 ^b	1	26.61	24.75	111
2.8879 2.8608 2.6853 2.6339 2.6049 ^b		· · • •	26.61	040
2.8608 2.6853 2.6339 2.6049 ^b		29.55		
2.6853 2.6339 2.6049 ^b	100	30.94	30.91	240
2.6339 2.6049 ^b	66	31.24	31.22	131
2.6049 ^b	52	33.34	33.30	311
	10	34.01	34.00	420
	1	34.40		
2.4245 ^b	1	37.05		
2.3364	38	38.50	38.47	331
2.2834 ^b	1	39.43		
2.2324	1	40.37	40.39	060
2.1742	42	41.50	41.47	151
2.0801	1	43.47	43.48	260
1.9878 ^b	3	45.60		
1.9718	13	45.99	45.96	002
1.9582	6	46.33		
1.9103	14	47.56	47.55	600
1.8920	6	48.05	48.04	022
1.8657	2	48.77	48.78	202
1.8361	17	49.61	49.57	620
1.8108	46	50.35	50.32	531
1.7975	3	50.75	50.76	222
1.7610	2	51.88	51.87	460
1.7413 ^b	2	52.51		
1.7096 ^b	2	53.56		
1.7026	3	53.80	53.81	171
1.6733	15	54.82	54.81	080
1.6599	2	55.30	55.32	640
1.6290	16	56.44	56.42	642
1.5934	9	57.82	57.82	551
1.5789	2	58.40	58.39	422
1.5696	13	58.78	58.79	371
1.5542 ^b	1	59.42		
1.511 7 ^b	1	61.27		
1.5037	1	61.63	61.65	711
1.4783	4	62.81	62.82	062
1.4624	11	63.57	63.59	442
1.4518	9	64.09	64.11	660
1.4422 ^b	3	64.57	-	
1.4327	15	65.05	65.05	731
1.4017	5	66.67	66.69	820
1.3731	11	68.25	68.28	602
1.3450	4	69.88	69.90	622

^a Calculated from an orthorhombic unit cell, a=11.466(2); b=13.389(2) and c=3.9458(6) Å.

(compare with fig. 3). The major differences between our new diagram and the one presented in [27] are: 1) the occurrence of a new compound which is estimated to have the stoichiometry $Sr_6Bi_2O_9$ (fig. 4a); 2) the presence of a high temper-

ature polymorph of $SrBi_2O_4$ (fig. 4b) which becomes stable between 800 and 825 °C and melts incongruently at 940 \pm 5 °C; and 3) the determination of melting relations in the region of 20–50 mol percent SrO.

^b Superstructure peak.

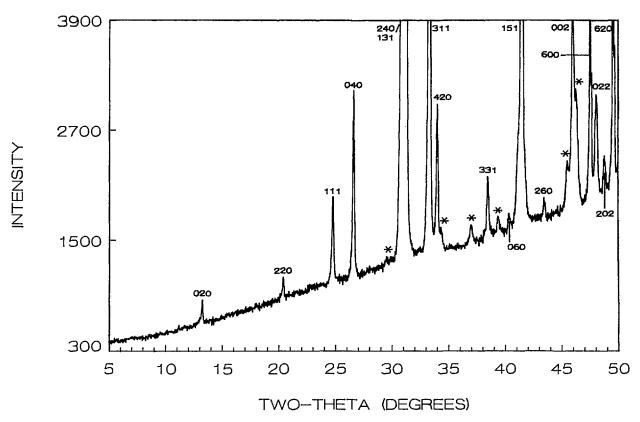


Figure 1. X-ray powder diffraction pattern of Sr₁₄Cu₂₄O₄₁ (cooled from 925 °C). *Superstructure peaks.

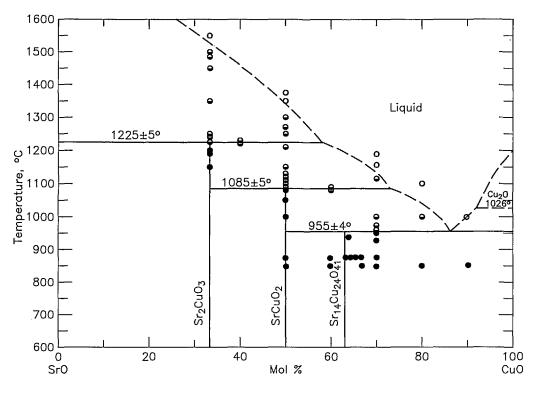


Figure 2. Phase diagram for the system SrO-CuO \(\begin{align*}\)-not melted, \(\omega\)-partially melted, \(\Omega\)-completely melted.

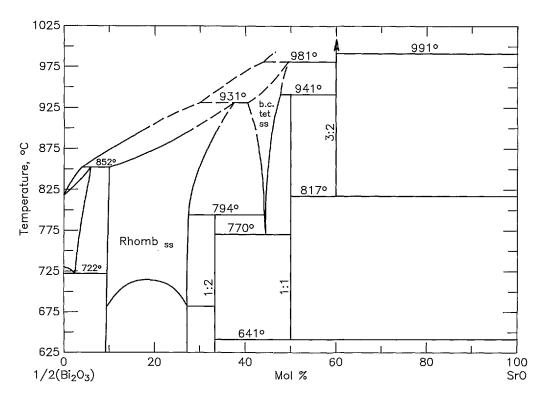


Figure 3. Phase diagram for the system SrO-¹₂Bi₂O₃ modified from that published in [27].

Solid Solution (Sillen 3.3.1 Rhombohedral Phase-Rhomb) The rhombohedral solid solution was first reported by Sillen [29] and it was later shown by Levin and Roth [30] that the solidus temperature is increased when SrO is added to facecentered-cubic (fcc) Bi₂O₃, or when it is added to the rhombohedral solid solution phase. Melting relations in the SrO-rich region of the Sillen phase field were previously [27] represented schematically (by dashed lines) as a melting loop, but the experiments reported in [28] indicate a congruent melting point between 25-30 mol% SrO and 950-960 °C. Guillermo et al. [27] reported that a phase transition occurred from one rhombohedral phase to another, but as this has not been confirmed by quench data, such possible polymorphism is ignored in the present work. X-ray diffraction data for this phase are well established [27] and will not be summarized here.

3.3.2 SrBi₂O₄ (SB₂) SrBi₂O₄ appears to have both high- and low-temperature polymorphs with a transition point at about 825 °C. The high-temperatures form melts incongruently to liquid plus the tetragonal solid solution (next section) between 940 and 945 °C. In the high to low-temperature transi-

tion, sharp x-ray diffraction peaks in a powder pattern of the low-temperature phase become broad and diffuse when specimens are quenched from about 825-940 °C. Also, a few maxima (e.g., 202) that are present in patterns from the low-temperature phase have drastically reduced intensities in patterns from samples that were quenched from above 825 °C. The indexed x-ray powder diffraction data for low-SrBi₂O₄ are listed in table 4. The patterns for both low-temperature and high-temperature SrBi₂O₄ are shown in figure 5. The observed broadening of diffraction maxima in the pattern from the quenched sample suggests that the high-temperature polymorph, perhaps orthorhombic, was not successfully quenched. The presence of broad rather than sharp peaks suggests a small domain size in samples quenched from above 825 °C.

Very small single crystals of low-temperature SrBi₂O₄ were prepared (table 1b) by heating a prereacted powder sample of SrBi₂O₄ plus a 1:1 NaCl:KCl flux (80/20 flux/charge ratio) in a sealed Pt tube. The specimen was heated to 740 °C and cooled to 570 °C at 6 °/h. After the flux was dissolved with H₂O, a very thin flat platelet was

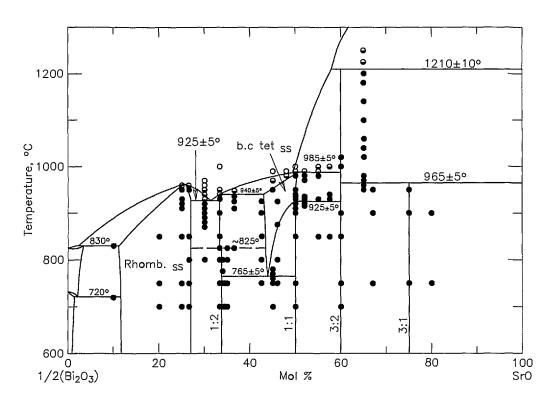


Figure 4a. Phase diagram for the system $SrO_{\frac{1}{2}}Bi_2O_3$ as reported in [28] \bullet -not melted, \ominus -partially melted, \bigcirc -completely melted.

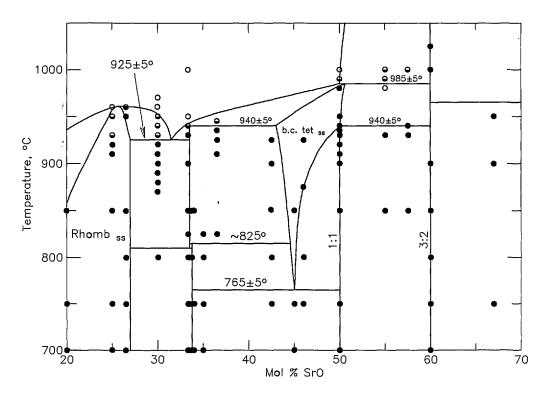


Figure 4b. Enlargement of figure 4a showing polymorphism of SrBi₂O₄.

Table 4. X-ray powder diffraction data for the compound SrBi₂O₄

d obs(Å)	Rel I(%)	2θ obs	2θ calc ^a	hkl
9.64	9	9.17	9.19	200
6.09	4	14.53	14.55	001
5.36	1	16.54	16.56	201
4.813	22	18.42	18.44	400
3.626	7	24.53	24.53	401
3.606	6	24.67	24.69	310
3.454	29	25.77	25.78	111
3.205	97	27.81	27.81	600
3.168	100	28.15	28.16	311
3.040	93	29.36	29.38	311
2.9743	15	30.02	30.03	202
2.9417	3	30.36	30.38	601
2.8326	6	31.56	31.57	202
2.7421	13	32.63	32.63	601
2.6728	7	33.50	33.51	511
2.5454	1	35.23	35.25	511
2.4781	7	36.22	36.23	402
2.4526	3	36.61	36.63	112
2.4051	1	37.36	37.38	800
2.3065	19	39.02	39.03	602
2.2724	5	39.63	39.64	312
2.1782	34	41.42	41.42	020
			42.59	711
2.1196	22	42.62	42.64	602
2.0501	1	44.14	44.13	021
2.0291	2	44.62	44.62	512
2.0197	3	44.84	44.86	$20\bar{3}$
1.9841	5	45.69	45.69	420
1.9686	5	46.07	46.07	802
1.9191	19	47.33	47.35	910
1.8701	33	48.65	48.63	91Ī
1.8427	8	49.42	49.40	113
1.8145	17	50.24	50.25	403
1.8018	43	50.62	50.63	620
	30	50.02	50.95	911
1.7909	16			022
1.7705		51.58	51.57	$\frac{022}{22\overline{2}}$
1.7569	11	52.01	52.00	
1.7318	9	52.82	52.81	313
1.7270	8	52.98	53.00	222
1.7096	10	53.56	53.53	513
1.7058	12	53.69	53.70	621
1.6812	3	54.54	54.54	912
1.6514	2	55.61	55.60	603
1.6357	5	56.19	56.18	422
1.6107	6	57.14	57.12	513
1.6023	11	57.47	57.45	12,0,0
1.5831	19	58.23	58.22	622
1.5691	7	58.80	58.77	912
1.5670	6	58.89	58.90	10,0,2

^a Calculated on the basis of a monoclinic cell, C2/m, a = 19.301(2), b = 4.3563(5), c = 6.1049(7) Å, $\beta = 94.85(1)^{\circ}$.

picked and single crystal x-ray precession photographs were taken (fig. 6) of it. The precession data indicate that the phase is C-centered monoclinic, probably C2/m, and unit cell dimensions refined from x-ray powder diffraction data

are a = 19.301(2), b = 4.3563(5), c = 6.1049(7) Å, $\beta = 94.85(1)^{\circ}$. Larger crystals were obtained from both 80:20 and 50:50 flux/charge ratios by cooling from 800 °C to 645 °C at 1°/h.

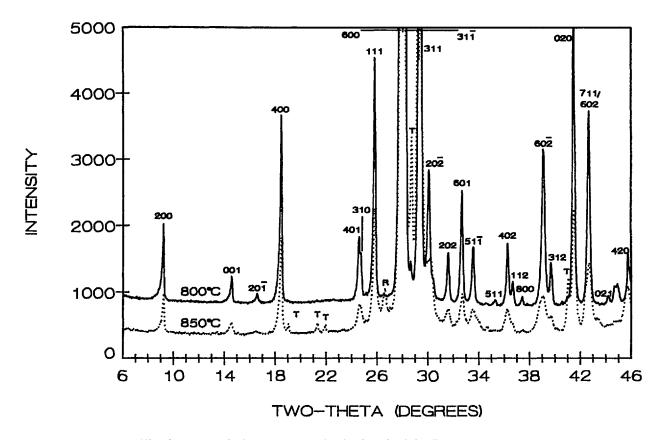


Figure 5. X-ray powder diffraction patterns for low-temperature (cooled from 800 °C) solid line and high-temperature SrBi₂O₄ (cooled from 850 °C) dotted line. T=tetragonal phase, R=rhombohedral phase.

3.3.3 The Tetragonal Solid Solution Near SrBi_{1,22}O_{2,83} (Tet) This phase was previously reported [27] with space group I4/m, a = 13.239(2), c = 4.257(1) Å. Experiments during the course of this study agree reasonably well with those previously reported, except for the region near the solidus where we find the single phase region extends to compositions with at least 50 mol percent SrO. The x-ray powder diffraction data was previously reported [27]. Very large single crystals were obtained by cooling the Sr₂Bi₂O₅ composition from above the melting point to ~ 950 °C.

3.3.4 $Sr_2Bi_2O_5(S_2B_2)$ The compound $Sr_2Bi_2O_5$ was reported [27] to be orthorhombic, space group Pemm with a = 14.293(2), b = 7.651(2) and c = 6.172(1) Å. Although precession photographs collected from very small crystals in the present study show evidence of only $\frac{1}{2}$ the b axis reported in [27] (see fig. 7), much larger crystals showed a very weak superstructure and a doubled b-axis. The subcell space group is apparently Cmcm and in this a = 3.8262(2), b = 14.307(1), orientation

6.1713(4) Å as obtained from a least-squares refinement of the powder data. The indexed powder data are given in table 5 and illustrated in figure 8. Apparently the superstructure destroys the subcell symmetry of the C-centering, showing such peaks as (1/2, 16, 0) and (1 1/2, 0, 1) resulting in a space group symmetry consistant with Pbnm. Very large single crystals were obtained by cooling the Sr₂Bi₂O₅ composition from above the melting point to ~900 °C, and annealing large fragments at 850 °C-258 h.

3.3.5 $Sr_3Bi_2O_6(S_3B_2)$ $Sr_3Bi_2O_6$ melts incongruently between 1200 and 1220 °C. Single crystals are formed in many compositions in the ternary system with CuO when heated above ~900 °C. Apparently, this phase has a large primary phase field in the ternary system. For example, single crystals were obtained from SrO: Bi₂O₃:CuO 55:35:10 at 900 °C and from $SrO_{\frac{1}{2}}Bi_{2}O_{3}$ 57.5:42.5 at 1000 °C. These crystals often react slowly with atmospheric moisture. The best crystals were obtained using an NaCl:KCl flux with 4/1 flux/Sr₆Bi₂O₉ ratio cooled

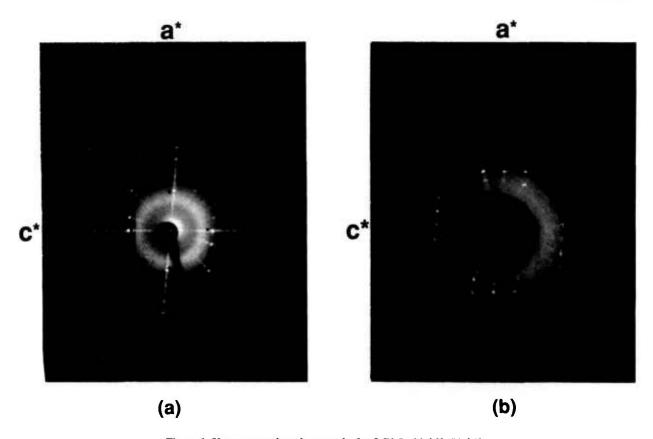


Figure 6. X-ray precession photographs for SrBi₂O₄ (a) h0l, (b) h1l.

from 1025 to 650 °C at 5 °/h (table 1b). These crystals are colorless and easily recognized because of their very low birefringence in polarized light. All these crystals were found (see precession photographs, fig. 9) to be rhombohedral probably $R\bar{3}m$, with unit cell dimensions refined from the x-ray diffraction powder data (table 6, fig. 10) a=12.526(1), c=18.331(2) Å.

3.3.6 Sr₆Bi₂O₉(S₃B) Previous workers [27] did not report any binary compound with more than 60 mole percent SrO; however, Sr₆Bi₂O₉ appears to be stable between about 750 and 950 °C, and it decomposes between 950 and 975 °C to Sr₃Bi₂O₆+SrO. Single crystals were obtained by heating a prereacted specimen plus 1:1 NaCl:KCl flux (flux/ charge ratio=10/90). X-ray precession photoindicate graphs (fig. 11) an apparently unit cell with a = 6.009 and rhombohedral c = 58.633 Å. This appears, however, to be a subcell and even a doubled a-axis (as suggested by electron diffraction data) does not account for all of the diffraction maxima observed in an x-ray powder diffraction pattern of the prereacted mix (table 7, fig. 12). The crystals may actually be an oxychloride phase and the pseudocell suggested in table 7 does not fit the observed data very accurately. The reaction $Sr_6Bi_2O_9 \rightarrow (975 \,^{\circ}C) \rightarrow Sr_3Bi_2O_6 + 3SrO$ is completely reversible i.e., with material that was decomposed, $Sr_6Bi_2O_9 \rightarrow Sr_3Bi_2O_6 + 3SrO$ at $975 \,^{\circ}C$, one can perform the back reaction, $Sr_3Bi_2O_6 + 3SrO \rightarrow (900 \,^{\circ}C) \rightarrow Sr_6Bi_2O_9$, with or without intermediate grinding (and exposure to atmospheric CO_2).

3.4 The System SrO: ¹/₂Bi₂O₃:CuO

Phase relations in the nominally ternary system are shown in figure 13 and experimental data are reported in table 1. Figure 14 is an enlargement of the triangular region of figure 13 that is delineated by dots. Many of the experiments listed in table 1 yield apparently conflicting and often confusing results, precisely because the experimental system is not strictly ternary in air and/or in contact with various capsule materials such as Au, Pt or 70Ag30Pd. Reproducibility of experiments in this system is exceedingly difficult to achieve, and it is often impossible to reproduce the results published

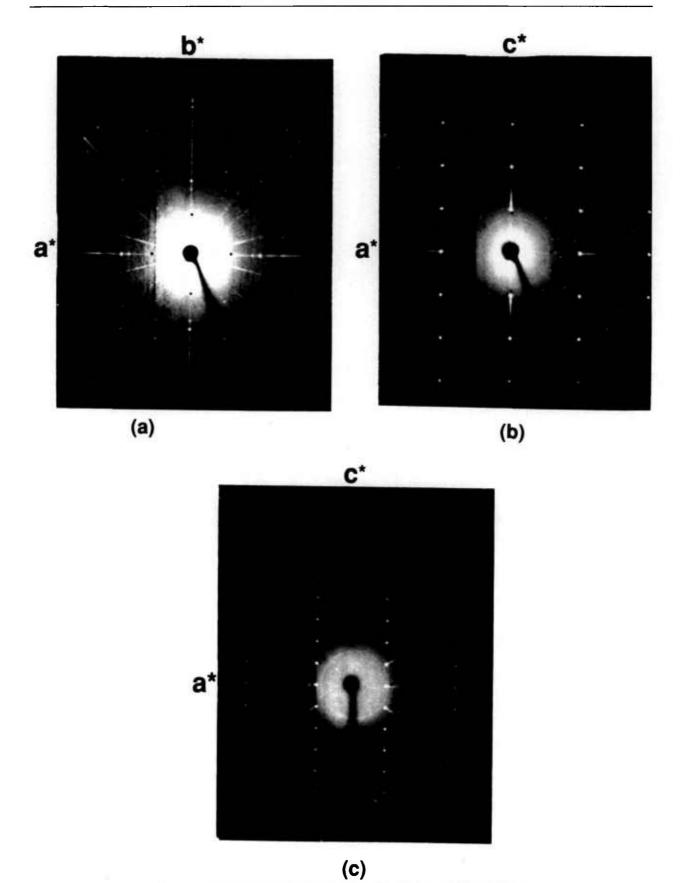


Figure 7. X-ray precession photographs of Sr₂Bi₂O₅ (a) hk0, (b) h0l and (c) h1l.

d obs(Å)	Rel I(%)	2θ obs	2θ calc ^a	hkl
7.161	17	12.35	12.3	020
4.676	15	18.96	18.98	021
3.697	32	24.05	24.06	110
3.171	1	28.11	28.12	111
3.094	100	28.84	28.83	041
2.9842	10	29.92	29.92	130
2.8319	8	31.57	31.55	022
2.6865	23	33.33	33.32	131
2.3857	1	37.67	37.69	060
2.3684	11	37.96	37.95	112
2.3373	<1	38.49	38.50	042
2.2918	9	39.28	39.29	150
2.2254	2	40.50	40.52	061
2.1466	26	42.06	42.09	132
1.9767	1	45.88	45.87	023
1.9122	8	47.51	47.49	200
1.8873	2	48.18	48.19	062
1.8401	8	49.50	49.51	152
1.8030	5	50.59	50.59	170
1.7979	8	50.74	50.75	113
1.7827	17	51.20	51.19	043
1.7712	2	51.56	51.58	221
1.7306	7	52.86	52.86	171
1.6936	5	54.11	54.10	133
1.6873	1	54.33	54.34	240
1.6271	17	56.51	56.51	241
1.5849	<1	56.16	58.14	222
1.5570	5	59.31	59.32	172
1.5472	7	59.72	59.71	082
1.5424	7	59.92	59.91	004

Table 5. X-ray powder diffraction data for the compound Sr₂Bi₂O₅

by others. In some cases this may be because insufficient experimental details were given; however, attempts to reproduce our own experiments have sometimes lead to slightly different results. Experimental results are greatly affected by the factors outlined below.

- (1) Compositional changes caused by reaction with Au or other containers;
 - (2) Volatilization of Bi₂O₃;
- (3) CO₂ in some phases at the lower temperatures (e.g., SrCO₃ does not decompose in air until about 875 °C);
- (4) Oxidation/reduction reactions involving atmospheric O₂, CO₂, or H₂O;
- (5) Difficulties related to the very disparate melting behaviors of various compounds and the end members. For example, Bi₂O₃ melts at ~825 °C but CuO decomposes in air to form Cu₂O at about 1020 °C which melts at about 1210 °C. Also, The Sr-cuprates react very slowly at temperatures below the melting points of Bi₂O₃ and Bi₂CuO₄. Thus, it was often necessary to prepare specimens from

prereacted compounds (or mixtures of compounds) instead of the end members.

(6) Persistence of apparently unstable three phase assemblages within single phase regions. Typically, it is not possible to homogenize single phase ternary samples to the point that all detectable traces of additional phases are eliminated from x-ray powder patterns.

Therefore, it should be emphasized that the diagram in figure 13 is a composite of subsolidus data that is neither strictly ternary nor strictly isothermal. The region below the join that connects CuO to the SrO-poor end of the rhombohedral Sillen phase field contains phases which melt below 850 °C, and some phases in the low CuO portion of the system begin to melt between ~875 and 900 °C. Also, specimens of one composition which are near the SrBi₂O₄:Raveau-solid-solution join showed evidence of melting between 850 and 875 °C. All other compositions start to melt above at least 900 °C and many start melting slightly above 925 °C.

^a Calculated on the basis of an orthorhombic unit cell, Cmcm, a = 3.8262(2), b = 14.307(1), c = 6.1713(4) Å.

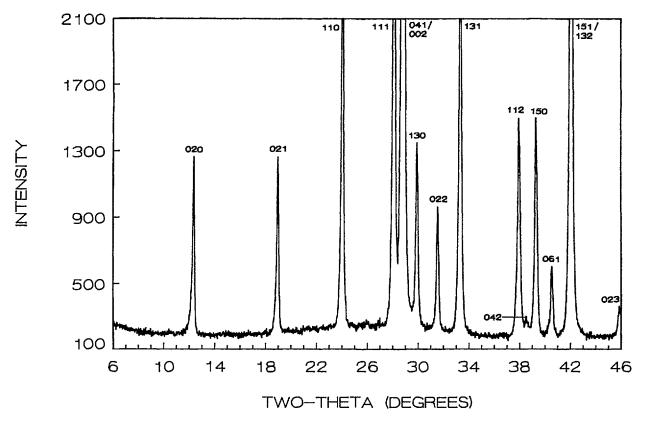


Figure 8. X-ray powder diffraction pattern of Sr₂Bi₂O₅ (cooled from 900 °C).

3.4.1 $Sr_2Bi_2CuO_6(S_2B_2C-2:2:1)$ This compound should nominally be the end member with n=1 of the homologous series $Sr_2Bi_2Ca_{n-1}Cu_nO_{2n+4}$. However, the x-ray powder diffraction pattern for this composition does not match at all with the predicted tetragonal subcell for a compound of this structure type. The predicted type of x-ray pattern is only found in specimens that are grossly deficient in SrO (i.e., compositions corresponding to the Raveau solid solution region—see below). The compound which occurs at approximately Sr₂Bi₂CuO₆ has been characterized by electron diffraction and x-ray powder and single crystal diffraction and the results reported elsewhere [18]. The compound was found to be monoclinic, space group C2/m (or Cm) with a = 24.493(2), b = 5.4223(5), c = 21.959(2) Å, $\beta = 105.40(1)^{\circ}$. The actual composition with Sr:Bi:Cu ratio of 2:2:1 always contains a small amount of Sr₁₄Cu₂₄O₄₁ and probably also some of the Raveau-type phase. Therefore, this compound is shown in figures 13 and 14 as being slightly deficient in CuO (less than 1 mol percent) and having a small homogeneity region. The x-ray powder diffraction data, single

crystal precession photographs and electron microscopy data, along with figure 14, were previously published [18]. This phase appears to have a subcell with c-subcell (~ 5.49 Å) $\frac{1}{4}c$ -supercell; electron microscopy data for some grains indicate an incommensurate superstructure. The x-ray diffraction data for compositions with only 19 mol percent CuO do not yield satisfactory least-squares refinements. It is possible that the observed incommensurate modulation is an equilibrium phenomenon dependent on composition, although it is equally likely to be due to a non-equilibrium chemical inhomogeneity.

3.4.2 The Raveau-Type Solid Solution (Rav) A two-phase region is shown in figure 14 (after [18]) between the 2:2:1 phase and the region referred to as the Raveau-type solid solution. This nomenclature is used because, structurally, the Raveau-type phase most closely resembles n=1end member of Sr₂Bi₂Ca_{n-1}Cu_nO_{2n+4} and because Raveau and coworkers were the first to report superconductivity in this system [31]. This phase often forms

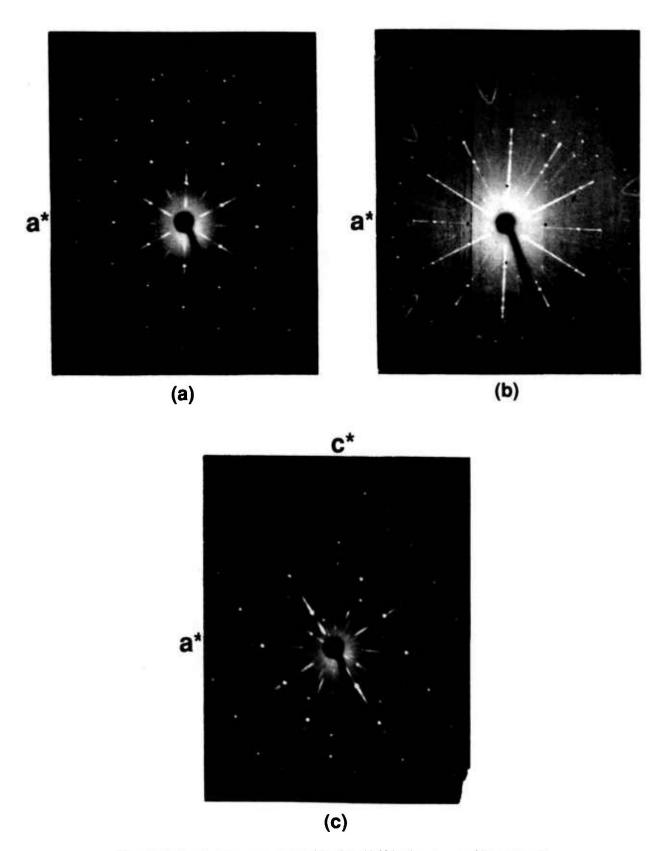


Figure 9. X-ray precession photographs of $Sr_3Bi_2O_6$ (a) hk0, (b) unscreened hk0 and (c) h0l.

Table 6. X-ray powder diffraction data for the compound Sr₃Bi₂O₆

d obs(Å)	Rel I(%)	2θ obs	2θ calc ^a	hkl
9.32	2	9.48	9.47	101
6.997	2	12.64	12.63	012
6.100	4	14.51	14.49	003
4.662	16	19.02	19.00	202
4.371	14	20.30	20.29	113
4.217	8	21.05	21.03	104
4.001	11	22.20	22.20	211
3.740	9	23.77	23.76	122
3.1326	100	28.47	28.48	220
3.0394	85	29.36	29.38	205
2.9694	6	30.07	30.08	131
2.8582	4 3	31.27	31.27	312
2.7861	2	32.10	32.09	223 116
2.7454	2	32.59 32.72	32.58 32.74	125
2.7347 2.6013	7	34.45	34.46	042
2.5150	8	35.67	35.67	134
2.4024	1	37.40	37,42	232
2.3588	26	38.12	38.13	027
2.3329	2	38.56	38.54	404
2.3265	2	38.67	38.68	315
2.2420	3	40.19	40.19	018
	-		{ 40.85	413
2.2073	5	40.85	40.86	217
2.1797	63	41.39	41.38	045
2.1552	2	41.88	41.90	051
0.1111	2	40.90	(42.79	502
2.1111	2	42.80	(42.81	208
2.0277	2	44.42	44.43	241
2.0377	2	44.42	\ 44.44	009
2.0011	11	45.28	45.29	422
2.0011	11	45.20	45.30	128
1.9767	6	45.87	∫ 45.90	333
1.9707	v	45.07	l 45.9 1	137
1.9376	7	46.85	{ 46.86	511
			46.87	119
1.9062	4	47.67	47.68	152
1.8832	12	48.29	48.27	407
1.8711	7	48.62	∫ 48.62	244
			48.62	416
1.8230	9	49.99	49.99	318
1.8087	24	50.41 51.00	50.44 51.00	600 425
1.7893	46	31.00	51.00 [51.44	423 431
1.7753	9	51.43	51.45	309
			52.21	342
1.7512	3	52.19	52.22	048
1.7367	40	52.66	52.66	0,2,10
1.7248	4	53.05	53.09	336
1.7240	4	53.21	53.20	155
1.6855	5	54.39	54.38	238
1.6146	9	56.99	57.00	247
1.5931	4	57.83	57.84	2,0,11
1.5667	24	58.90	58.94	440
			(59.35	164
1.5569	5	59.31	59.35	606
			(59.85	701
1.5443	9	59.84	,	

^a Calculated on the basis of a rhombohedral unit cell a=12.526(1), c=18.331(2) Å.

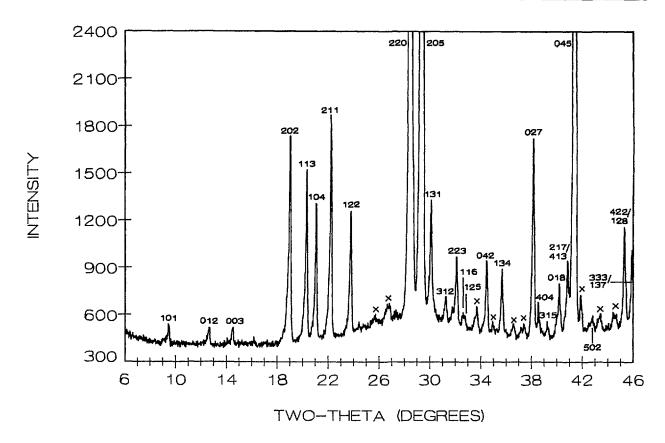


Figure 10. X-ray powder diffraction pattern of Sr₃Bi₂O₆ (cooled from 975 °C). X=unidentified peaks-probably due to hydration.

metastably as an almost single-phase product when compositions near the indicated equilibrium singlephase region are synthesized by cooling from a melt. For example, a melt of 2:2:1 composition first crystallizes as the Raveau solid solution and reacts to form the 2:2:1 phase only after subsequent heating and grinding (table 1); similarly, when a mixture of composition 3:2:2 was prepared by a lactate route, the Raveau solid solution was the first crystalline phase to form; but, the 3:2:2 phase replaced it after subsequent heating and grinding (table 1). The crystals formed from melts of Raveau solid solution, or similar compositions (outside the equilibrium Raveau field), are always very platy and micaceous and form "books" of crystals not well ordered in the direction perpendicular to the plates. They always have one long crystallographic axis of about 26.6 Å and the x-ray powder diffraction data can be roughly fit to a pseudotetragonal subcell with a = 5.3 Å. Several unit cells have been reported for this phase, either pseudotetragonal or pseudoorthorhombic [32,33].

Crystals that were picked from various ternary melts (with or without chloride flux) were invariably non-single and appear to have a monoclinic

superstructure. The phase formed using 1:1 NaF:KF flux, however, yielded crystals with apparent orthorhombic symmetry and a very strange incommensurate superstructure (fig. 15). Onoda and Sato [34] obtained a monoclinic superstructure for a crystal that was grown from a melt of 1:1:1 composition (Sr:Bi:Cu=1:1:1) which was heated in an Al₂O₃ crucible. They report a nominal composition for the crystal of Sr:Bi:Cu 4:6:3, well outside the equilibrium single-phase region reported in figures 13 and 14. The unit cell reported for this phase [34] is C-centered monoclinic with a = 26.856, b = 5.380, c = 26.908 Å, $\beta = 113.55^{\circ}$; no data were reported on the extent of contamination from the Al₂O₃ crucible. A calculated powder pattern based on their structure determination [34] was obtained from M. Onoda (private communication) and these data were used to index the x-ray powder diffraction pattern of the composition with Sr:Bi:Cu ratios of 36:44:20 (near the SrO-rich end of the Raveau solid solution region). All of the superstructure lines observed for this composition can be completely accounted for by hkl's with intensities very similar to those calculated by Onoda, For a C-centered monoclinic cell, the unit cell dimen-

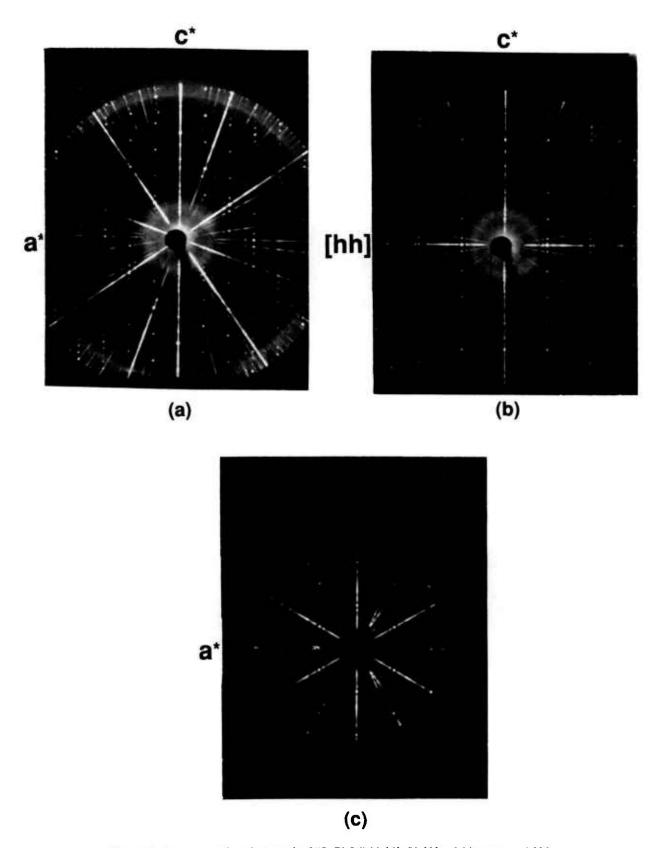


Figure 11. X-ray precession photograph of " $Sr_6Bi_2O_9$ " (a) h0l, (b) hhl and (c) unscreened hk0.

Table 7. X-ray powder diffraction data for the compound Sr₆Bi₂O₉

d obs(Å)	Rel I(%)	2θ obs	2θ calc ^a	hklb
4.891	18	18.12	18.13	0,0,12
4.777	1	18.56		
4.397	1	20.18		
4.258	12	20.85	20.93	018
4.197	6	21.15		
3.810	1	23.33		
3.589	1	24.79		
3.396	3	26.22	26.13	1,0,13
3.318	1	26.85		
3.271	1	27.24		
3.218	1	27.70		
3.184	1	28.00		
3.092	1	28.85	20.71	140
3.0105	58	29.65	29.74	110
2.9997	61	29.76	29.79	1,0,16
2.9859	100	29.90		
2.8779	1	31.05		
2.8493	1	31.37		
2.7283	1	32.80	22 =4	1010
2.6437	5	33.88	33.74	1,0,19
2.5615	16	35.00	35.05	1,1,12
2.5357	9	35.37		
2.4827	2	36.15	26-4	
2.4436	4	36.75	36.74	0,0,24
2.4075	1	37.32		
2.3829	2	37.72		
2.3672	2	37.98		
2.3383	1	38.55		
2.2974	1	39.18	20.00	0.0.12
2.2603	6	39.85	39.99	0,2,13
2.2308	1	40.40	42.60	0.2.16
2.1272	32 15	42.46 43.14	42.00	0,2,16
2.0953 2.0452	2	44.25		
2.0432 2.0146	1	44.96		
1.9952	4	45.42		
1.9845	3	45.68		
1.9550	4	46.41		
1.9502	6	46.53		
1.9415	8	46.75		
1.9337	10	46.95		
1.9054	4	47.69		
1.9006	5	47.82		
1.8629	4	48.85		
1.8452	2	49.35		
1.8118	2	50.32		
1.8001	3	50.67		
1.7509	3	52.20		
1.7364	18	52.67		
1.7318	35	52.82	52.77	300
1.7188	21	53.25	22	200
1.7031	2	53.78		
1.6838	2	54.45		
1.6557	2	55.45		
1.6354	9	56.20		
1.6295	4	56.42		
1.6156	3	56.95		
1.5884	1	58.02		
1.5802	2	58.35		

^a Calculated on the basis of a rhombohedral subcell with a = 6.009, c = 58.663 Å.

^b Based on the intensities observed in single crystal precession photographs, figure 11.

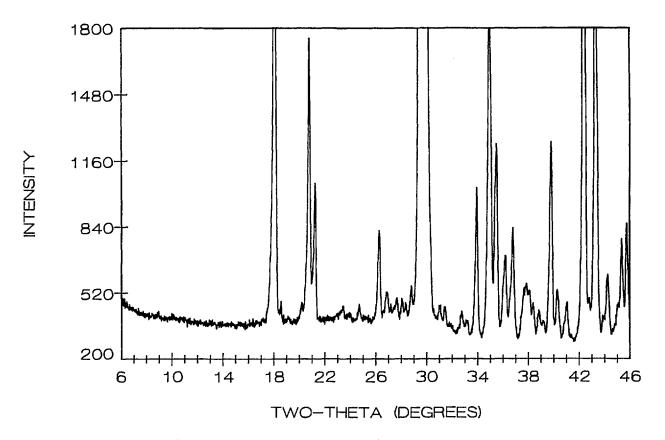


Figure 12. X-ray powder diffraction pattern of $Sr_6Bi_2O_9$ (heated to 975 °C then cooled to 900 °C, held for 24 h and cooled to room temperature).

sions obtained by least-squares analysis of this x-ray powder data (table 8, fig. 16) are a = 26.889(9), b = 5.384(2), c = 26.933(8) Å, $\beta = 113.67(3)^{\circ}$.

It should be noted, however, that powder patterns for more Bi-rich Raveau-type solid solutions display superstructure peaks which deviate widely from those observed for the 36:44:20 composition. At present it is not known if this is truly a region of solid solution or a collection of smaller regions (separated by two and/or three phase fields) in which several structurally related phases are stable. New specimens are currently being prepared at very close intervals in this Raveau-type region in order to determine the true crystal chemistry of this important "phase." These results will be reported in the near future [35].

The Raveau solid solution region extends along a line with approximately 20 mol percent CuO according to the formula $Sr_{1.8-x}Bi_{2.2+x}CuO_z$ with $\sim 0.0 < x < \sim 0.15$. This is slightly at odds with the results of Saggio et al. [36] who reported the formula $Sr_{1.8+x}Bi_{2.2-x}CuO_z$ with 0.0 < x < 0.08 which corresponds to negative values of x in our formula.

Their samples were annealed at 800 °C and premixed with 0.5 weight percent Li₂CO₃. It is not known if the differences between their results and ours are due to the temperature difference, the time of "equilibration," or to the presence of Li₂CO₃. They also report [36] that only the high SrO end of the solid solution exhibits superconductivity based on the data of Akimitsu et al. [37] which were obtained from specimens that were heated twice at 880 °C for 12 h. This preparation should probably have yielded results similar to ours, but we failed to find evidence of superconductivity at temperatures above 10 K. It is possible that superconductivity only occurs in metastable Raveau-type solutions that have compositions which lie outside the equilibrium "single phase" field.

The Raveau-type solid solution also exhibits non-stoichiometry with respect to its CuO concentration. The solid solution region corresponds approximately to the formula $Sr_{1.8-x}Bi_{2.2+x}Cu_{1\pm x/2}O_z$. Of course, there is no *a priori* reason why the CuO concentration must be structurally controlled by the Sr/Bi ratio.

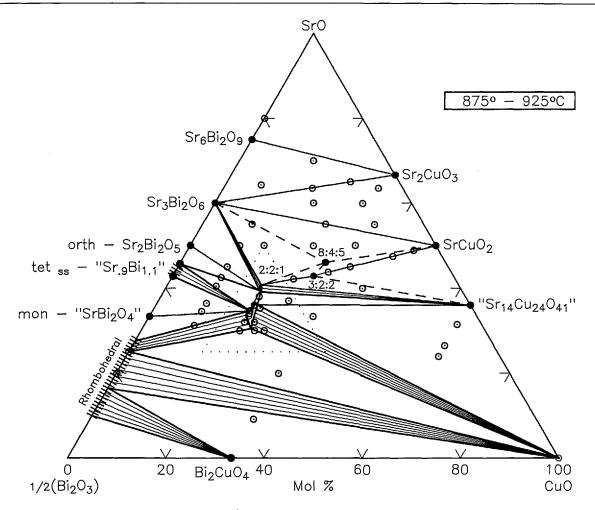


Figure 13. Phase diagram for the system SrO-½Bi₂O₃-CuO. O-compositions studied, ●-compounds. This diagram represents subsolidus conditions, although Bi₂O₃ melts at 825 °C and therefore partial melting occurs below 875 °C in most compositions below the join CuO-Rhomb. In addition, some melting was found at 875 °C for the composition 34.66:55.33:10.

Chakoumakos et al. [38] reported the results of a study of Raveau-type single crystals that were grown under oxygen from CuO-rich melts in crucibles of various compositions. Incomensurate superstructure peaks (related to orthorhombic symmetry) were found to vary systematically with the SrO content. Superconductivity was found to be related to excess oxygen and to the concentration of impurities including Al₂O₃. The superstructure peaks occurred with modulation of $\sim 1/5b^*$ plus a c* component varying from 0.29c* to 0.65c* (where * represents the reciprocal vector direction). The observed formula for these crystals was reported as Bi₂Sr_{2-x}CuO_{6-v}. These crystals (and most if not all melt-grown, Raveau-type crystals) are probably metastable since they have compositions well outside the equilibrium range shown in figures 13 and 14. It should be noted, however, that Chakoumakos et al. grew their crystals under oxygen rather than air, so the relevant single-phase region may be similar but will not be identical to that in figures 13 and 14.

3.4.3 $Sr_8Bi_4Cu_5O_{19+x}$ ($S_8B_4C_5$ -8:4:5) This phase was apparently first described [39] as a compound with the composition Sr₄Bi₂Cu₂O_{9+z} (Sr:Bi:Cu=2:1:1); however, an examination of the reported unindexed x-ray powder diffraction data indicate that modest amounts of both S₁B₂ and SC were present in this sample. All of our experiments with the 2:1:1 composition yielded three phases when equilibrated in air at subsolidus temperatures, although the minority phases that were observed depended upon the heat treatment (table 1). Small single crystals of this new phase were obtained from a specimen of 2:1:1 that was mixed with 10 weight percent 1:1 NaCl:KCl flux and sealed in a gold tube that was heated at 900 °C for 1 h then cooled to 650 °C at 3 °C/h. The crystals are needlelike suggesting that one crystallographic axis is

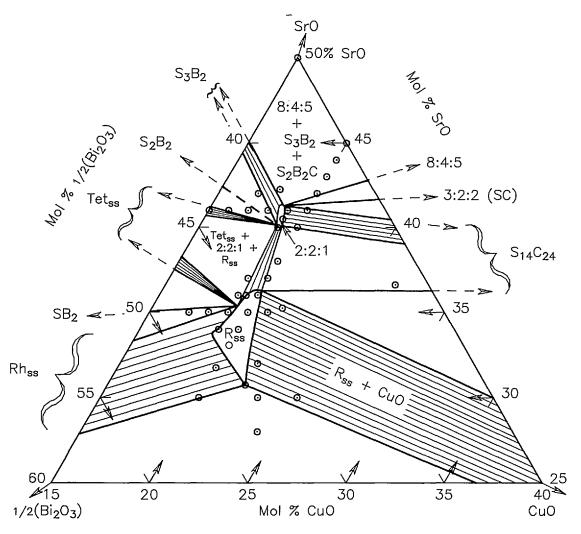


Figure 14. An enlargement of the triangular region of the phase diagram in figure 13 that is delineated by dots.

probably much shorter than the others, and x-ray precession photographs (fig. 17) revealed that it is orthorhombic (space group Fmmm) with a, b, c parameters of approximately 33.98, 24.02, 5.364 Å, respectively. The crystal structure of this phase has been solved by Fuertes et al. [40] who describe its chemistry as $\text{Bi}_4\text{Sr}_8\text{Cu}_5\text{O}_{19+x}$, and its unit cell as orthorhombic with a=5.373(2), b=33.907(6), c=23.966(4) Å. Obviously, the diffraction data in figure 17 indicate that this is the same phase as the one reported in [39,40].

Single-phase specimens of $Sr_8Bi_4Cu_5O_{19+x}$ were only obtained in this laboratory when the starting materials were annealed in one atmosphere of oxygen. The unit cell refined from the data obtained from the 8:4:5 specimen (table 9, fig. 18) is orthorhombic Fmmm with a=33.991(3), b=24.095(2), c=5.3677(5). Clearly the published

structure of this phase [40] requires more than the 19 oxygen atoms per formula unit that are implied by an 8:4:5 ratio. The smaller unit cell obtained by [40] was also found in the present work when an 8:4:5 specimen was melted in an Al₂O₃ crucible (as were the crystals reported by [40]) poured onto an Al plate and annealed in air or oxygen. Attempts to supply the excess oxygen by the substitution of some La⁺³ for some of the Sr⁺² as suggested by R. J. Cava (private communication) was only partially successful, never resulting in a completely single-phase specimen when heated in air.

3.4.4 $Sr_3Bi_2Cu_2O_8$ ($S_3B_2C_2$ -3:2:2) Extrapolation based on the general formula for the homologous series of Bi-containing high- T_c phases, $A_2Ca_{n-1}B_2Cu_nO_{2n+4}$, predicts the formula $Sr_2CaBi_2Cu_2O_8$ (2:1:2:2) for the phase with n=2, and a c-axis of ~ 30.6 Å which implies d(002)

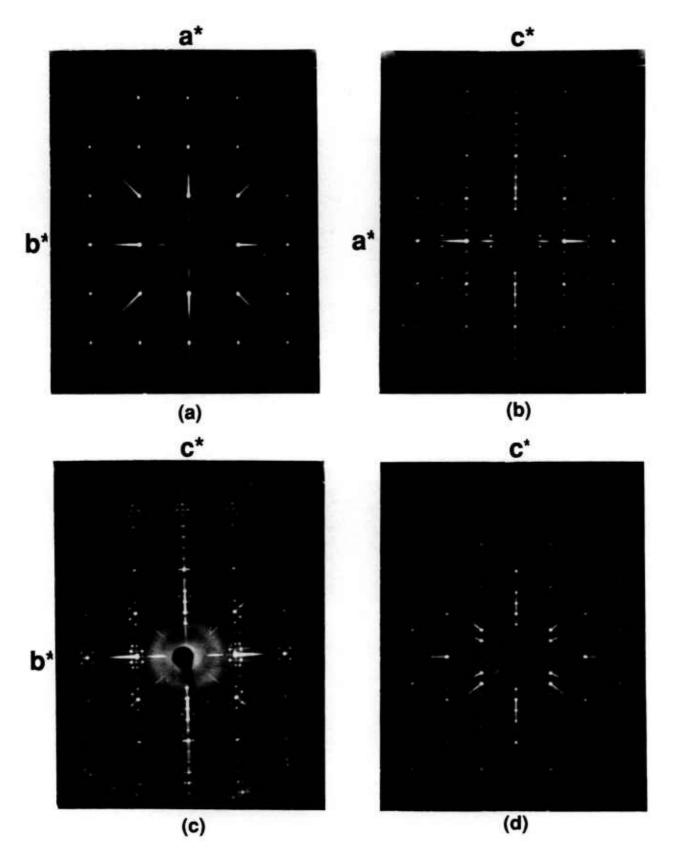


Figure 15. X-ray precession photographs of an orthorhombic/incommensurate Raveau solid solution phase that was grown in 1:1 NaF:KF flux. Original composition=Sr₂Bi₂CuO₆ (a) hk0, (b) h0l, (c) 0kl and (d) hhl.

Table 8. X-ray powder diffraction	data for the Raveau-type phase at the	;
composition Sr _{1.8} Bi _{2.2} CuO _{6.1} a		

d obs(Å)	Rel I(%)	2θ obs	2θ calc ^b	hkl°
12.35	6	7.15	7.17	200
6.16	1	14.37	14.38	400
5.47	1	16.20	16.17	401
5.26	3	16.83	16.84	110
4.50	1	19.70	19.70	310
4.348	2	20.41	20.44	601
4.183	2	21.22	21.22	114
4.105	34	21.63	21.63	600
	•	00.64	[23.62	315
3.761	2	23.64	23.62	115
		24.40	24.45	514
3.632	4	24.49	24.47	510
			25.76	515
3.457	58	25.75	25.78	115
3.384	1	26.32	26.32	116
3.239	4	27.52	27.50	517
3.220	6	27.68	27.70	801
3.092	24	28.85	28.85	714
3.081	66	28.96	28.96	800
			[29.62	715
3.013	100	29.63	29.64	315
2.9427	5	30.35	30.32	710
2.9380	5	30.40	30.41	209
2.9025	11	30.78	30.81	716
2.7929	3	32.02	32.05	514
2.7462	2	32.58	32.54	316
	_		[33.24	4,0,10
2.6924	58	33.25	33.25	020
			(34.04	6,0,10
2.6317	2	34.04	34.05	2,0,10
			34.06	220
2.5831	7	34.70	(34.68	915 915
	•	0	34.70	515
2.5560	2	35.08	35.11	10,0,1
2.4623	15	36.46	36.45	10,0,0
2.4481	5	36.68	36.71	4,0,11
2.4182	5	37.15	37.15	6,0,11
2.3565	5	38.16	38.12	10,0,1

^a Oxygen content not certain.

~5.78° 2θ for CuK α radiation. It is known that Sr⁺² can substitute for some of the Ca⁺² up to at least 3:3:4:4 [40]. If all the Ca⁺² were replaced by Sr⁺², the chemical formula would degenerate to 3:2:2 or Sr₃Bi₂Cu₂O₈; but, attempts to synthesis the n=2 phase at this composition have failed. The presence of a small peak at ~5.75° 2θ was noted during the first low temperature calcination of specimens prepared by decomposition of lactate precursor powders with 3:2:2 composition. However, the peak at ~5.75° 2θ disappears after subsequent heat treatments which suggests that it is associated with a metastable phase.

Compositions of 3:2:2 prepared by conventional solid state techniques yield a new phase that has an x-ray powder diffraction pattern (table 10, fig. 19) which resembles both the Raveau-type solid solution and the 2:2:1 phase in some respects. The low angle peak occurs at about the same value as for the Raveau solid solution ($d \sim 12.35 \text{ Å}$, $2\theta \sim 7.15^\circ$), but there is a very small peak at a d-value of twice that ($d \sim 24.7 \text{ Å}$, $2\theta \sim 3.58^\circ$). The strong (113) Raveau-type tetragonal subcell peak at $\sim 25.75^\circ$ 2θ is not present and, instead, a strong peak occurs at $\sim 26.85^\circ$ 2θ , similar to the 2:2:1 compound. In addition, there are considerable differences between

^b Calculated from monoclinic unit cell a = 26.889(9), b = 5.384(2), c = 26.933(3) Å, $\beta = 113.67(3)^{\circ}$.

^c Indexed based on single crystal F_{obs} data received from M. Onoda [34].

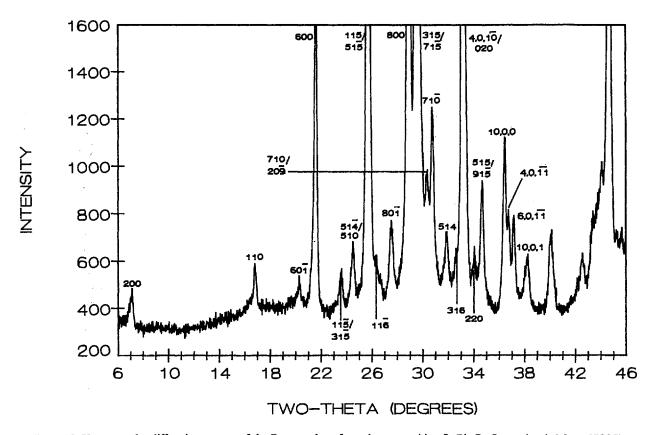


Figure 16. X-ray powder diffraction pattern of the Raveau phase from the composition Sr₉Bi₁₁Cu₅O_{30.5±x} (cooled from 875 °C).

this pattern and both the Raveau solid solution and $Sr_2Bi_2CuO_6$, which indicate that $Sr_3Bi_2Cu_2O_8$ is a unique phase. As yet, no single crystals of this phase have been synthesized. The pattern in figure 19 shows the presence of a small amount of $Sr_{14}Cu_{24}O_{41}$, indicating some probable nonstoichiometry in the composition. The diffraction maxima in this pattern have been indexed with comparison to the 2:2:1 and Raveau solid solution with a C-centered monoclinic unit cell, a=24.937(7), b=5.395(2), c=19.094(7) Å, and $\beta=96.97(3)^{\circ}$. This commensurate cell probably represents only a subcell of an incommensurate non-stoichiometric phase.

3.4.5 Miscellaneous Phases of Unknown Composition Two phases high in SrO content at approximate Sr:Bi:Cu ratios of 9:4:1 and 7:2:2 were reported by Saggio et al. [36], and two different phases at 4:2:1 and 2:1:1 were reported by Casais et al. [39]. Of these, we only found evidence for the phase reported at 7:2:2 composition, and then only at temperatures below 875 °C. The Saggio et al. data [36] are complicated by their use of the 0.5 wt% Li₂CO₃ "as a mineralizer." Peaks correspond-

ing to the d-spacings reported for the composition 9:4:1 were not present in our specimens except when we included 0.5 wt% Li₂CO₃, and the binary phase Sr₆Bi₂O₉ (that was not reported by Saggio et al. [36]) is only present when Li₂CO₃ is absent. We therefore conclude that the "9:4:1-phase" is not present in the ternary system. Some of the low-angle d-spacings reported for the "7:2:2-phase" (4.82 $\mathring{A}=18.40^{\circ} 2\theta$ and $4.17 \mathring{A}=21.27^{\circ} 2\theta$) in samples that were heated at 800 °C were observed in patterns from samples that we heated at temperatures below ~875 °C (table 1). Because SrCO₃ does not decompose until ~ 875 °C, these results suggest the presence of one or more oxycarbonate phases. The first two d-spacings as well as the strongest peak reported as a "4:2:1" phase [38] (d = 4.91, 4.25 and 3.004 Å) are apparently due to the phase $Sr_6Bi_2O_9(S_3B)$.

In summary, we interpret the evidence for these four reported phases as follows:

9:4:1-mostly due to reaction with Li₂CO₃; 7:2:2-multiphase due to reaction with Li₂CO₃ plus a Sr:Bi:Cu-oxycarbonate;

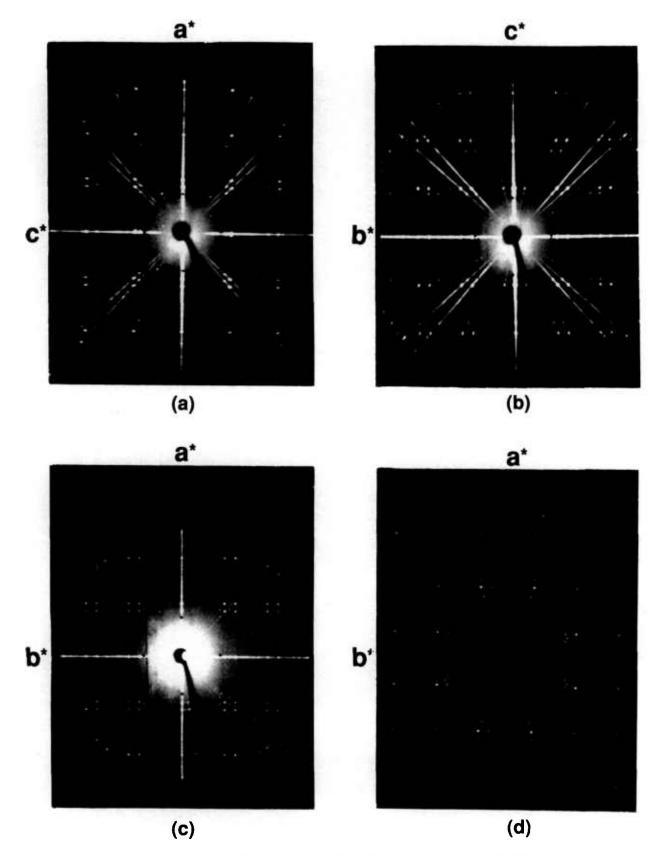


Figure 17. X-ray precession photographs of 8:4:5 (a) h0l, (b) 0kl, (c) hk0 and (d) hk1.

Table 9. X-ray powder diffraction data for the compound Sr₈Bi₄Cu₅O_{19+x}^a

d obs(Å)	Rel I(%)	2θ obs	2θ calc ^b	hkl°
17.05	3	5.18	5.20	200
12.08	3	7.31	7.33	020
9.85	1	8.97	8.99	220
5.668	<1	15.62	15.63	600
4.425	2	20.05	20.05 20.89	131
4.253 4.153	2 2 4	20.87 21.38	21.39	800 511
4.015	4	22.12	22.12	060
3.911	3	22.72	22.73	260
3.729	13	23.84	23.83	531
3.559	1	25.00	24.98	711
3.418	2	26.05	26.04	351
3.288	33	27.10	27.12	731
3.173	23	28.10	28.11	551
3.011	27	29.65	29.64	080
2.9665	. 4	30.10	30.11	280
2.8861	100	30.96	30.95	171
2.8317	11	31.57	31.56	12,0,0
2.7569	2	32.45	32.44	12,2,0
2.6837	35 1	33.36 33.80	33.36 33.78	002 202
2.6498 2.6182	3	34.22	33.76 34.20	022
2.0102	4	34.40 ^d	34.20	022
2.5903	i	34.60	34.62	222
2.4881	2	36.07	36.07	771
2.4264	27	37.02	37.00	14,0,0
2.4080	24	37.31	37.29	0,10,0
2.3793	3	37.78	37.77	14,2,0
2.3417	1	38.41	38.42	11,5,1
2.3145	1	38.88	38.88	12,6,0
2.2571	2	39.91	39.93	13,3,1
2.2303	1	40.41	40.39	062
2.2125	1 2	40.75	40.75	262
2.1485 2.12 44	4	42.02 42.52	42.02 42.52	791 16.0.0
2.1244	3	42.75	42.77	16,0,0 13,5,1
2.0639	14	43.83	43.84	12,8,0
2.0077	14	45.12	45.12	0,12,0
2.0036	14	45.22	45.22	082
1.9474	24	46.60	46.58	12,0,2
1.9443	23	46.6 8	46.70	5,11,1
1.9164	20	47.40	47.42	15,5,1
1.8909	2	48.08	48.10	14,8,0
1.8715	21	48.61	48.61	7,11,1
1.8351	8	49.64	49.63	12,10,0
1.8001	19	50.67	50.66	14,0,2
1.7935	21	50.87	50.89	0,10,2
1.7875	12	51.05 52.15	51.08	9,11,1
1.7525 1.7494	3 4	52.15 52.25	52.14 52.24	12,6,2 1,13,1
1.7264	3	53.00	53.02	513
1.7099	9	53.55	53.54	14,10,0
1.6967	7	54.00	54.01	5,13,1
1.6915	7	54.18	54.18	533
1.6604	10	55.28	55.28	19,3,1
1.6478	27	55.74	55.73	7,13,1
1.6437	21	55.89	55.90	733
1.6359	10	56.18	56.18	12,8,2
1.6288	5	56.45	56.46	553
1.6007	25 26	57.53	57.53	19,5,1
1.5851	26	58.15	58.14	753
1.5453	13	59.80	∫ 59.79 50.81	14,8,2
			[59.81	22,0,0

^a Oxygen content based on structure derived by [40].

d SrCuO₂.

^b Calculated by least-square analysis from orthorhombic unit cell, Fmmm, a = 33.991(3), b = 24.095(2), c = 5.3677(5) Å.

o Indexed with the aid of the single crystal precession photographs, figure 17 and intensities calculated from the published structure [40].

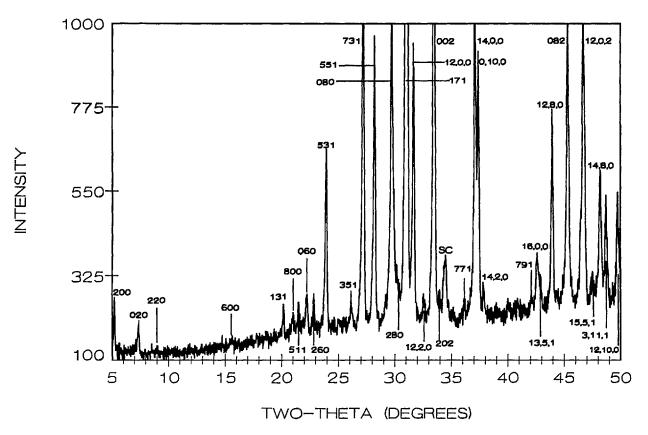


Figure 18. X-ray powder diffraction pattern of Sr₈Bi₄Cu₅O_{19+x} (cooled from 925 °C in O₂).

4:2:1-Sr₆Bi₂O₉+other phases; and 2:1:1-Sr₈Bi₄Cu₅O_{19+x}+S₃B₂+SC

On heating above about 850 °C, the diffraction maxima characterizing the 7:2:2 "phase" start to disappear and are ultimately replaced by at least one other strong maximum at $\sim 30.25^{\circ}$ 2θ the origin of which is still unknown. At the 3:1:1 composition (table 1) the 7:2:2-type phase is very prevalent at 750 and 800 °C; however, as it starts to decompose at 850 °C, another peak arises at $\sim 11.00^{\circ}$ 2θ which persists even at 900 °C after the first heat treatment but finally disappears after three overnight anneals. The origin of this $\sim 11.00^{\circ}$ peak is also unknown but it appears to indicate a metastable phase that forms during decarbonation and subsequently decomposes.

At the 2:1:1 and 8:4:5 compositions it was found that preliminary low-temperature annealing was actually detrimental to the formation of an equilibrium assemblage. Apparently, an oxycarbonate phase characterized by small peaks at $2\theta = 4.40^{\circ}$ and 5.60° with strong peaks at 30.50° and 32.45° is formed first with repeated heating at 750°C; further heat treatments at 800 °C produce a new peak at

 \sim 4.80° as the 4.40° peak gradually disappears. These are gradually replaced by peaks from the 2:2:1 and Raveau solid solution plus $SrCuO_2$, but the 8:4:5 phase which should form is not found. Note, however, that when this sample was put in an Al_2O_3 crucible, melted and reheated at 900 °C, the 8:4:5 phase did form. Apparently, the formation of these oxycarbonates blocks the nucleation of 8:4:5.

Four ternary phases were reported in this system by Ikeda et al. [42]. These are essentially the same phases as those reported here, although the compositions do not always agree. The formula given for the Raveau phase solid solution differs somewhat from that used here. The formula for Sr₂Bi₂CuO₆ is given as Sr₁₆Bi₁₇Cu₇O₂, considerably deficient in SrO and occurring in the region clearly shown by our work to contain three phases. The x-ray diffraction pattern shown for their Sr₃Bi₂Cu₂O₂ clearly shows evidence of the Sr₁₄Cu₂₄O₄₁ phase, as do our own patterns of this composition. Unit cell dimensions and symmetry given by Ikeda et al. [42] and Saggio et al. [36] for their ternary phases are clearly based on intuition rather than single crystal data and should be considered suspect.

Table 10.	X-ray	powder	diffraction	data	for	the	compound	Sr ₃ Bi ₂ Cu ₂ O ₈ ^a
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d obs(Å)	Rel I(%)	2θ obs	2θ calc ^b	hkl
24.7°	1	3.57		
12.35	3	7.15	7.14	200
5.26	2	16.84	16.81	110
5.12	1	17.32	17.33	111
4.120	10	21.55	21.52	600
4.064°	2	21.85		
3.992	2	22.25	22.22	113
3.625	9	25.54	24.54	602
3.573	2	24.90	24.92	114
3.315	48	26.87	26.86	604
3.124	11	28.55	28.63	115
3.095	33	28.82	28.83	800
3.053	2	29.20	29.23	802
3.043	2	29.33	29.32	513
2.9220	100	30.57	30.57	803
2.8031	1	31.90	31.79	315
2.7082	26	33.05	33.06	007
2.6963	60	33.20	33.19	020
2.6324	4	34.03	34.04	714
2.5581	2	35.05	35.07	222
2.5518	2	35.14	35.11	805
2.5281	3	35.48	35.56	222
2.4748	20	36.27	36.26	10,0,0
2.4384	16	36.83	36.85	912
2.3933	3	37.55	37.55	317
2.2571	3	39.91	39.91	317
2.0993	2	43.05		
2.0629	5	43.85		
2.0334	34	44.52		
1.9877	4	45.60		
1.9815	3	45.75		
1.9125	41	47.50		
1.8919	2	48.05		
1.8539	2	49.10		
1.8239	13	49.96		
1.8090	14	50.40		
1.7908	3	50.95		
1.7875	2	51.05		
1.7360	5	52.68		
1.7232	3	53.10		
1.6857	18	54.38		
1.6532	12	55.54		
1.6388	4	56.07		
1.6279	18	56.48		
1.5971	24	57.67		
1.5744	19	58.58		
1.5620	8	59.09		
1.5475	6	59.70		

 $^{^{\}text{a}}$ Heated to 925 $^{\circ}\text{C}$ in flowing O_2 on Au foil. Total oxygen content uncertain.

3.4.6 Deduction of Ternary Compatibility (Alkemade) Lines This ternary system is remarkable for the gross irreproducibility of the experimental results. Attainment of equilibrium for each of the ternary compounds that we represent as stable is

very difficult and time consuming. Nevertheless, equilibrium can generally be more easily achieved in ternary combinations furthest from the compositions of the stable ternary phases. For this reason the deduction of the compatibility joins is some-

^b Calculated on the basis of a C-centered monoclinic cell with a=24.937(7), b=5.395(2), c=19.094(7) Å, $\beta=96.97(3)^{\circ}$.

^c Superstructure peaks.

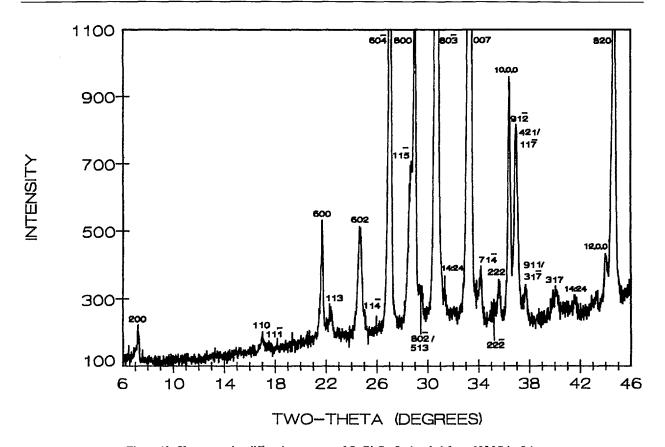


Figure 19. X-ray powder diffraction pattern of Sr₃Bi₂Cu₂O₈ (cooled from 925 °C in O₂).

what more reliable than one might suppose based on the difficulties inherent in determining the true compositions of the ternary phases.

Some generalizations can be made concerning both the data in table 1 and the interpretations behind our construction of figures 13 and 14. Because there is a two phase region involving CuO and the rhombohedral Sillen-phase solid solution, the compound Bi₂CuO₄ and the low melting eutectics of the Bi₂O₃-CuO binary system are not involved in most of the ternary equilibria. Also, CuO is in equilibrium with most or all of the compositions comprising the Raveau-type solid solution region. Therefore, the 1:1:1 composition (reported by Raveau [31] as superconducting) is in the middle of a ternary phase field bounded by CuO, Raveau solution and S₁₄C₂₄. The compound solid Sr₁₄Cu₂₄O₄₁ is in equilibrium with all three of the ternary phases related to the structurally homologous series $A_2Ca_{n-1}B_2Cu_nO_{2n+4}$: $Sr_2Bi_2CuO_6$, $Sr_3Bi_2Cu_2O_8$ and $Sr_{1.8-x}Bi_{2.2+x}Cu_{1\pm x/2}O_2$ (i.e., 2:2:1, 3:2:2 and the Raveau solid solution), but not with the structurally dissimilar phase Sr₈Bi₄Cu₅O_{19+z} (8:4:5) or any of the SrO-Bi₂O₃ binary phases. The compound SrCuO2 is in equilibrium with all three

of the ternary compounds except for the Raveautype solid solution while Sr₂CuO₃ is compatible only with the two high SrO content binary phases but not with any of the ternary phases. Joins describing compatibility conditions for the 8:4:5 and 3:2:2 phases are left as dashed lines because of the difficulty in determining equilibrium three phase assemblages.

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